

**SOME ROBUST RIDGE ESTIMATORS: A COMPARATIVE STUDY**

Abdulrasheed Bello Badawairea*, Kayode Ayindeb, M. L. Danyaroc, Umar A. Ahmedd

* Department of Mathematics & Statistics, Federal University Wukari, Nigeria

Department of Statistics, Federal University of Technology Akure, Nigeria

Department of Basic Science, Yobe State College of Agriculture Gujba, Nigeria

Department of Basic Science, Taraba State College of Agriculture Jalingo, Nigeria

DOI: 10.5281/zenodo.3591003**KEYWORDS:** Multicollinearity, Outlier(s), Robust Ridge, Robust Generalised Ridge.**ABSTRACT**

In the presence of multicollinearity and outliers, the Ordinary Least Square estimator is found to be inefficient due to the inflated standard errors. In this paper, some forms of Generalized Ridge regression parameters proposed by Fayose and Ayinde (2019) were combined with robust estimators to estimate the parameters of linear regression model when multicollinearity and outliers are jointly evident. Linear regression models with three and five regressors ($p = 3$ and $p = 5$), three levels of multicollinearity ($\rho = 0.900, 0.990$ and 0.999), three levels of percentages of outliers ($n1\% = 5\%, 10\%$ and 20%), three levels of magnitude of outliers ($\sigma_{outliers}^2 = 10, 100$ and 250) and three levels of sample size ($n = 20, 40$ and 100) were considered through Monte Carlo experiments. The experiments were carried out 1000 times, and the performances of these combined estimators and Ordinary Least Square were investigated and compared using the Mean Square Error (MSE) criterion. Results show that the Maximum form of Fayose and Ayinde's modified Generalized Ridge parameter of Troskie and Chalton (1996) when combined with robust Least Absolute Deviation estimator ($\hat{\alpha}_{LADFA1}^{max}$) consistently performed more efficiently than all other methods of parameter estimation of linear regression model considered. It also shows that increasing the sample size, the number of explanatory variables, degree of multicollinearity, the magnitude of outliers and percentage of outliers affect the efficiency of these estimators.

INTRODUCTION

Ordinary Least Squares (OLS) estimator is the most popular estimator used in estimating the parameters of the linear regression model. This estimator is the Best Linear Unbiased Estimator when all the assumptions of the Classical Linear Regression Model are met (Fonby, 1984; Maddala, 2002).

One of the problems encountered in regression analysis is the existence of outlier(s) in a dataset which is one of the violations in the classical linear regression model. Outlier(s) renders the OLS residuals to be non-normal. Consequently, the OLS estimator will be inefficient, and the estimates obtained from it will be imprecise as a result of the inflated error variance (Ayinde et al., 2015). The following estimation techniques are developed to handle the problems of outliers; M estimator proposed by Huber (1964), MM estimator proposed by Yohai (1987), S estimator proposed by Rousseeuw and Yohai (1984), LAD estimator proposed by Dielman (1984), LTS proposed by Rousseeuw, P. J. and Van Driessen, K. (1998). Different researchers such as Neykov and Neytchev (1991), Atkinson and Weisberg (1991), Stronberg (1993), Rousseeuw and Van Driessen (1999), Agullo (2001), Jung (2005), Li (2005), Cizek (2005) and Rousseeuw and Van Driessen (2006) also suggested different algorithms for computing the LTS estimates.

Multicollinearity is another problem encountered when estimating the parameters of the linear regression model using OLS. It arises when two or more predictors move precisely in step with each other (Murray, 2006). If multicollinearity exists in a dataset, the OLS estimator will be inefficient due to the inflated variance. Multicollinearity can as well lead to erroneous conclusions and can render the actual regression coefficients insignificant (Chatterjee and Hadi, 2006; Chatterjee et al., 2000). Estimators to handle this problem includes Stein estimator (Stein, 1960), Ridge regression estimator (Hoerl and Kennard, 1970), Principal Components Regression estimator (Massy, 1965), Partial Least Squares Regression estimator (Wold, 1966), and Least Absolute Shrinkage and Selection Operator (LASSO) proposed by Tibshirani (1996), Liu estimator (2003), modified ridge-type estimator (Lukman et al. 2019) and others.



Global Journal of Engineering Science and Research Management

Multicollinearity and outlier problem can exist together in a dataset. Research works done to handle these problems jointly includes robust M estimator for ridge regression proposed by Holland (1973), robust regression methods based on M, MM, S, and GM estimators proposed by Samkar and Alpu (2010), ridge regression with M, MM, S, LTS, LMS and LAD introduced by Lukman et al., (2014), Ridge Least Absolute Value Estimator proposed by Pfaffenberger & Dielman (1990), Ridge MM estimator proposed by Habshah & Marina (2007), ridge regression based on robust MM estimator for high dimensional data developed by Maronna (2011).

This article aims to investigate the performances of some ridge regression estimators when combined with some robust regression estimators to combat the problems of outliers and multicollinearity in a linear regression model.

MATERIALS AND METHODS

Consider the standard linear regression model of the form:

$$Y = X\beta + U \quad (1)$$

where Y is an $n \times 1$ random vector of dependent variable, X is an $n \times p$ matrix with full rank, β is a $p \times 1$ vector of estimable parameters, and U is an $n \times 1$ random vector of residuals distributed as $N(0, \sigma^2 I_n)$. The Ordinary Least Squares estimator of β is

$$\hat{\beta}_{OLS} = (X'X)^{-1}X'Y \quad (2)$$

Let T be an orthogonal matrix, satisfying $T'X'XT = \Lambda = \text{diag}(\lambda_1, \lambda_2, \dots, \lambda_p)$, where Λ is a diagonal matrix of order $p \times p$ with diagonal elements $\lambda_1, \lambda_2, \dots, \lambda_p$ as the eigen values of $X'X$. T and Λ are the matrices of eigen vectors and eigen values, respectively. Hence, the canonical form of model (1) is:

$$Y = Z\alpha + U \quad (3)$$

where $Z = XT$ and $\alpha = T'\beta$.

Hence, the OLS estimator of α is:

$$\hat{\alpha}_{OLS} = \Lambda^{-1}Z'Y \quad (4)$$

2.1 Robust Estimators

M Estimator

M-estimator proposed by Huber (1964) perform parameter estimation by minimizing the sum of a less rapidly increasing function of the residuals. It performs better when the outliers are in the y-direction but less robust to leverage. The objective function of M estimate is given by:

$$\min \sum_{i=1}^n \rho \left(\frac{U_i}{s} \right) = \min \sum_{i=1}^n \rho \left(\frac{Y_i - Z'_i \hat{\alpha}_i}{s} \right) \quad (5)$$

where s is the scale estimate obtained as function of residuals and is estimated by

$$S = \frac{\text{median}|U_i - \text{median}(U_i)|}{h} \quad (6)$$

When n is large, an appropriate choice of h makes S an approximately unbiased estimator of σ .

To minimize (5), a system of normal equations is solved by taking partial derivative with respect to β and equating them to zero, which gives

$$\sum_{i=1}^n X_i \psi \left(\frac{Y_i - Z'_i \hat{\alpha}_i}{s} \right) = 0 \quad (7)$$

Where ψ is ρ' and Z_i is the i^{th} observation. Then Iterative Reweighted Least Squares (IRLS) or nonlinear optimization techniques is used to solve these equations.

MM-Estimator

MM- estimator proposed by Yohai (1987), is the combination of the high breakdown value estimator and M-estimator. By this estimator, parameter estimates are obtained from multiple M-estimation that uses the S-estimation procedure to minimize the scale of the residuals. The procedure involved the following three stages:



Global Journal of Engineering Science and Research Management

1. Initial estimates $\hat{\alpha}^{(1)}$ found using a high breakdown point estimator are used to compute the initial residuals $U_i^{(1)}$.
2. M-estimate of the scale of residuals S_n are computed using the initial estimate of residuals $U_i^{(1)}$ in step 1.
3. M-estimates of regression coefficients are obtained from Weighted Least Squares (WLS) whose first iteration uses the residual scale S_n from step 2 and the estimates of residuals $U_i^{(1)}$ from step 1

$$\sum_{i=1}^n Z_i W_i \left(\frac{U_i^{(1)}}{S_n} \right) = 0 \quad (8)$$

4. Residuals from the initial Weighted Least Squares (WLS) in step 3 are used to construct new weights, which again is used in Weighted Least Squares estimation. The process is continually reiterated until convergence.

S-Estimator

S-estimator proposed by Rousseuw and Yohai (1984), is a high breakdown value that minimize the dispersion of residuals. S-estimator minimize the dispersion in residuals as the solution of

$$\frac{1}{n} \sum_{i=1}^n \psi \left(\frac{U_i}{s} \right) = K \quad (9)$$

Where K is a constant.

Least Trimmed Squares Regression Estimator

Another estimator proposed by Rousseuw (1984), is the Least Trimmed Squares (LTS) regression. It is also a high breakdown value method that minimizes the sum of the trimmed squared residuals. LTS estimator is

$$\hat{\alpha}_{LTS} = \operatorname{argmin}(\sum_{i=1}^h U_i^2) \quad (10)$$

Where h is defined in the range $\frac{n}{2} + 1 \leq h \leq \frac{3n+P+1}{4}$, n and P representing sample size and number of parameters in the model.

Least Absolute Deviation Estimator

Least Absolute Deviation (LAD) regression proposed by Dielman (1984) is very resistant to observations with unusual Y values. Estimates are obtained by minimizing the sum of the absolute values of the residuals.

$$\min \sum_{i=1}^n |U_i| = \min \sum_{i=1}^n |Y_i - Z_i \hat{\alpha}| \quad (11)$$

LAD fails to account for leverage (Mosteller and Turkey 1977), and thus has a breakdown point of zero.

Generalized Ridge Estimator

The Generalized Ridge estimator of α is given by:

$$\hat{\alpha}_{GR} = [I - K(\Lambda + K)^{-1}] \hat{\alpha}_{OLS} \quad (12)$$

Where $K = \operatorname{diag}(k_1, k_2, \dots, k_p)$, is a p x p diagonal matrix whose elements k_1, k_2, \dots, k_p are the p different ridge parameters corresponding to p different regressors considered. Therefore, the Generalized Ridge estimator of β is

$$\hat{\beta}_{GR} = T \hat{\alpha}_{GR} \quad (13)$$

The mean square error of Generalized Ridge estimator is:

$$MSE(\hat{\alpha}_{GR}) = \sigma^2 \sum_{i=1}^p \lambda_i / (\lambda_i + k_i)^2 + \sum_{i=1}^p k_i^2 \hat{\alpha}_i^2 / (\lambda_i + k_i)^2 \quad (14)$$

While the MSE of $\hat{\alpha}_{OLS}$ is given by:

$$MSE(\hat{\alpha}_{OLS}) = \sigma^2 \sum_{i=1}^p 1/\lambda_i \quad (15)$$



Global Journal of Engineering Science and Research Management

The generalized ridge parameters used in this study are those proposed by Fayose and Ayinde (2019).

Fayose and Ayinde (2019) proposed some generalized ridge parameters by taking the Minimum (MIN), Maximum (MAX), Mid-Range (MID), Arithmetic Mean (AM), Median (MD), Geometric Mean (GM) and Harmonic Mean (HM) of eigen values (λ_i) of $X'X$ matrix to(of) the ridge parameter estimators proposed by Nomura (1988), Troskie and chalton (1996), Firinguetti (1999), Batach *et. al* (2008), Dorugade (2016) and Lukman and Ayinde (2017).

The estimators of generalized ridge parameters used in this study are the modification of Troskie and Chalton (1996) and Firinguetti (1999) by Fayose and Ayinde. The generalize ridge parameter by Troskie and Chalton is:

$$k_{TC} = \lambda_i \sigma^2 / (\lambda_i \hat{\alpha}_i^2 + \sigma^2) \quad (16)$$

While that of Firinguetti is computed as:

$$k_F = \lambda_i \sigma^2 / (\lambda_i \hat{\alpha}_i^2 + (n - p) \sigma^2) \quad (17)$$

Where n is the sample size and p is the number of independent variables in the model.

Hence, the generalized ridge parameters used are:

$$k_{FA1}^{min} = \lambda_{min} \sigma^2 / (\lambda_{min} \hat{\alpha}_i^2 + \sigma^2) \quad (18)$$

Where λ_{min} = minimum (λ_i), $i= 1, 2, \dots, p$

$$k_{FA1}^{max} = \lambda_{max} \sigma^2 / (\lambda_{max} \hat{\alpha}_i^2 + \sigma^2) \quad (19)$$

Where λ_{max} = maximum (λ_i), $i= 1, 2, \dots, p$

$$k_{FA1}^{mid} = \lambda_{mid} \sigma^2 / (\lambda_{mid} \hat{\alpha}_i^2 + \sigma^2) \quad (20)$$

Where $\lambda_{mid} = (\lambda_{max} + \lambda_{min}) / 2$

$$k_{FA1}^{md} = \lambda_{md} \sigma^2 / (\lambda_{md} \hat{\alpha}_i^2 + \sigma^2) \quad (21)$$

Where λ_{md} = median (λ_i), $i= 1, 2, \dots, p$

$$k_{FA1}^{gm} = \lambda_{gm} \sigma^2 / (\lambda_{gm} \hat{\alpha}_i^2 + \sigma^2) \quad (22)$$

Where $\lambda_{gm} = (\lambda_1 \times \lambda_2 \times \dots \times \lambda_p)^{\frac{1}{p}}$

$$k_{FA1}^{hm} = \lambda_{hm} \sigma^2 / (\lambda_{hm} \hat{\alpha}_i^2 + \sigma^2) \quad (23)$$

Where $\lambda_{hm} = p / \sum_{i=1}^p \frac{1}{\lambda_i}$.

Following a similar fashion, these forms are again applied to equation (17).

Robust Generalized Ridge Estimator

The robust generalized ridge estimator used in this study that jointly solve the problems of multicollinearity and outliers is given by

$$\hat{\alpha}_{RGR} = [I - K_{RobustFA}(\Lambda + K_{RobustFA})^{-1}] \hat{\alpha}_{Robust} \quad (24)$$

Where $K_{RobustFA}$ are the Fayose and Ayindes' generalized ridge parameters computed from robust (M, MM, S, LTS, LMS and LAD) estimates instead of the usual OLS estimates, and $\hat{\alpha}_{Robust}$ is the robust (M, MM, S, LTS, LMS, LAD) estimator of the model parameters.

$$\text{e.g, } k_{RobustFA1}^{min} = \lambda_{min} \sigma_{Robust}^2 / (\lambda_{min} \hat{\alpha}_{Robust}^2 + \sigma_{Robust}^2) \quad (25)$$

$$k_{RobustFA2}^{min} = \lambda_{min} \sigma_{Robust}^2 / (\lambda_{min} \hat{\alpha}_{Robust}^2 + (n - p) \sigma_{Robust}^2). \quad (26)$$

Where equation (25) and (26) are the robust minimum forms of Fayose and Ayinde's modified ridge parameters of Troskie and Chalton (1996) and Firinguetti (1999) respectively.

**Simulation Study**

In this paper, a Monte-Carlo experiment was carried out. The relation that yield the predictant is:

$$Y = X\beta + U \quad (27)$$

The procedure adopted by [20] and Kibria (36) was used to generate the predictors, the procedure is:

$$X_{ti} = (1 - \rho^2)^{\frac{1}{2}}Z_{ti} + \rho Z_{tp} \quad (28)$$

Where Z_{ti} are the standard normal and independently distributed random variables, each with mean zero and unit variance, ρ is the degree of relationship between any two predictors, which is varied as $\rho = (0.900, 0.990, 0.999)$ so as to study the effect of variation in degrees of multicollinearity.

The error term was simulated to have a Gaussian mixture, i.e. $U_t \sim (1 - n1\%)N(0,1) + n1\%N(0, \sigma_{outliers}^2)$. Where $n1\% = (5\%, 10\%, 20\%)$ were the percentages of outliers injected into the data, and $\sigma_{outliers}^2 = (10, 100, 250)$ is the magnitude of outliers considered.

The number of predictors were varied as $p = (3, 5)$ so as to study the impact of increase in number of predictors in the model. When $p = 3$, the true parameter values were fixed as: $\beta_1 = 0.8, \beta_2 = 0.1, \beta_3 = 0.6$, and when $p = 5$, $\beta_1 = 0.6, \beta_2 = 0.3, \beta_3 = 0.2, \beta_4 = 0.15$ and $\beta_5 = 0.7$, such that $\beta'\beta = 1$ in both cases.

To investigate the impact of sample size on the performance of these estimators, three sample sizes were considered, $n = 20, 40, 100$.

This experiment is replicated 1000 times and at each stage, the MSE is computed. The MSE of all the estimators is average over the number of replications and parameters as:

$$AMSE(\hat{\beta}) = \frac{1}{1000} \sum_{i=1}^p \sum_{j=1}^{1000} (\hat{\beta}_{ij} - \beta_i)^2. \quad (29)$$

This criterion was used in investigating the performances of these estimators.

DISCUSSION OF RESULTS

The average of the estimated MSE of OLS and seventy-two (72) other robust generalized ridge estimators over the number of parameters of a varying number of predictors at different sample sizes, the magnitude of outliers, levels of multicollinearity and percentage of outliers are presented in Table 1 to Table 9 at the Appendix. From Table 1 to Table 9, we observed that, at a fixed magnitude of outliers, number of explanatory variables, levels of multicollinearity and percentage of outliers, as sample size increase, the AMSE of the estimators' decreases. The AMSE of the estimators increases with an increase in the magnitude of outliers.

Also, AMSE increases as the number of explanatory variables increase and as levels of multicollinearity increases. $\hat{\alpha}_{LADFA1}^{max}$ Consistently has the smallest values of AMSE, even though $\hat{\alpha}_{LADFA1}^{mid}$ compete with it favourably. OLS consistently has the largest values of AMSE, at all the levels of sample size, magnitude of outliers, number of explanatory variables, levels of multicollinearity and percentage outliers considered.

CONCLUSION

In this study, the performances of some forms of Generalized Ridge parameters proposed by Fayose and Ayinde (2019) when combined with Robust estimators to jointly combat the problems of multicollinearity and outliers were evaluated and compared using the MSE criterion.

From the simulation study, it's found that the maximum form of Fayose and Ayinde's modified generalized ridge parameter by Troskie and Chalton (1996) when combined with robust LAD estimator outperformed all other methods of estimating the unknown regression parameters and is therefore, recommended as the most suitable estimator among the various estimators considered, when jointly faced with the problems of multicollinearity and outliers.



REFERENCES

1. Agullo, J. (2001), 'New algorithms for computing the least trimmed squares regression estimator', *Computational Statistics and Data Analysis* 36(4), 425–439.
2. Atkinson, A. & Weisberg, S. (1991), simulated annealing for the detection of multiple outliers using least squares and least median of squares fitting, in W. Stahel & S. Weisberg, eds, 'Directions in Robust Statistics and Diagnostics', Springer-Verlag, New York.
3. Ayinde, K., Lukman, A. F. and Arowolo, O.T. (2015). Robust regression diagnostics of influential observations in linear regression model. *Open Journal of Statistics*, 5, 1-11.
4. Batah, F., Ramanathan, T. and Gore, S. (2008). The efficiency of modified Jackknife and Ridge Type Regression Estimators: A Comparison, *Surveys in Mathematics and its Applications*, 24(2), F. 157 – 174.
5. Belsley, D. A., Kuh, E., & Welsch, R. E. (1980). *Regression Diagnostics: Identifying Influential Data and Sources of Collinearity*. Wiley Series in probability and Mathematical Statistics. New York: John Wiley & Sons.
6. Chatterjee, S. and Hadi, A.S. 2006. *Regression by Example*. 4th Edition, A Wiley-Interscience Publication, John Wiley and Sons.
7. Chatterjee, S., Hadi, A.S. and Price, B. 2000. *Regression by Example*. 3rd Edition, A Wiley-Interscience Publication, John Wiley and Sons.
8. Cizek, P. (2005), 'Least trimmed squares in nonlinear regression under dependence', *Journal of Statistical Planning and Inference* 136(11), 3967–3988.
9. Dorugade, A. V. (2014). New Ridge Parameters for Ridge Regression. *Journal of the Association of Arab Universities for Basic and Applied Sciences*, 15(1), 94 – 99.
10. Firinguetti, L. A (1999). Generalized Ridge Regression Estimator and its Finite Sample Properties. *Communications in Statistics. Theory and Methods* 28(5), 1217 – 1229.
11. Fomby, T. B., Hill, R. C. and Johnson, S. R. 1984. *Advance Econometric Methods*. Springer-Verlag, New York, Berlin, Heidelberg, London, Paris, Tokyo.
12. Habshah Midi & Marina Zahari. "A Simulation Study on Ridge Regression Estimators in the Presence of Outliers and Multicollinearity." *Jurnal Teknologi*. 47(C): 59-74, 2007.
13. Helland I. S. 1990. Partial least squares regression and statistical methods. *Scandinavian Journal of Statistics*, 17, 97 – 114.
14. Holland, P. W. (1973). Weighted ridge regression: Combining ridge and robust regression methods. NBER Working Paper Series 11, 1-19.
15. Hoerl, A. E. & Kennard, R.W. "Ridge Regression Biased Estimation for Nonorthogonal Problems", *Technometrics*, Vol.12, 55-67, 1970.
16. Huber, P. H. 1964. "Robust estimation of location parameter." *The Annals of Mathematical Statistics*, 35 7 101.
17. Jung, K. (2005), 'Multivariate least-trimmed squares regression estimator', *Computational Statistics and Data Analysis* 48(2), 307–316.
18. Li, L. (2005), 'An algorithm for computing exact least-trimmed squares estimate of simple linear regression with constraints', *Computational Statistics and Data Analysis*, 48(4), 717–734.
19. Lukman, A.F, Arowolo, O. and Ayinde, K. (2014). Some robust ridge regression for handling multicollinearity and outlier. *International Journal of Sciences: Basic and Applied Research* 16(2), 192-202.
20. Lukman, A.F, and Ayinde, K. (2017). Review and Classifications of the Ridge Parameter Estimation Techniques. *Haccettepe Journal of Mathematics and Statistics*, 46 (5), 953 – 967.
21. Lukman, A. F., Ayinde, K., Binuomote, S. and Onate, A. C., (2019). Modified ridge-type estimator to combat multicollinearity: Application to chemical data. *Journal of Chemometrics*, e3125.
22. Maddala, G. S. 2002. *Introduction to Econometrics*. 3rd Edition, John Wiley and Sons Limited, England.
23. Maronna, R.A. "Robust Ridge Regression for High-Dimensional Data." *Technometrics*, 53(1): 44- 53, 2011.
24. Massy, W.F. (1965). Principal Components Regression in exploratory statistical research. *J. Am. Stat. Assoc.*, 60, 234-256.
25. Murray, M. P. (2006), *Econometrics A Modern Introduction*. Boston: Addison-Wesley.



Global Journal of Engineering Science and Research Management

26. Neykov, N. & Neytchev, P. (1991), ‘Least median of squares, least trimmed squares and S estimations by means of BMDP3R and BMDPAR’, *Computational Statistics Quarterly* 4, 281–293.
27. Nomura, M. (1988). On the Almost Unbiased Ridge Regression Estimator. *Communication in Statistics – Simulation and Computation*, 17(3), 729 – 743.
28. Pfaffenberger, R. C., & Dielman, T. E. “A comparison of regression estimators when both multicollinearity and outliers are present.” In *Robust regression: Analysis and applications*, K. Lawrence & J. Arthur (Eds.), 243-270. New York: Marcel Dekker, 1990.
29. Phatak, A. and Jony, S. D. 1997. The geometry of partial least squares. *Journal of Chemometrics*, 11, 311 – 338.
30. Rousseeuw, P. J. & van Driessen, K. (1999), ‘A fast algorithm for the minimum covariance determinant estimator’, *Technometrics* 41(3), 212–223.
31. Rousseeuw, P. & van Driessen, K. (2006), ‘Computing LTS regression for large data sets’, *Data Mining and Knowledge Discovery* 12(1), 29–45.
32. Rousseeuw p. j., and Yohai, 1984. “Robust regression by means of S estimators in Robust and Nonlinear Time Series Analysis”, Franke J. Hardle, W. and Martin, R. D. *Lecture Notes in Statistics*, 26, New York: Springer-Verlag 256 - 274.
33. Rousseeuw, P. J. and Van Driessen K., “Computing LTS for Large Data Sets.” Technical Report, University of Antwerp, submitted, 1998.
34. Samkar, H. and Alpu, O. (2010). Ridge regression based on some robust estimators. *Journal of Modern Applied Statistical Methods*: 9(2), 495-501.
35. Stein, C. M. (1960). *Multiple Regression, Contributions to Probability and Statistics*, Stanford University Press, 424-443.
36. Stromberg, A. (1993), ‘Computing the exact least median of squares estimate and stability diagnostics in multiple linear regression’, *SIAM Journal on Scientific Computing* 14(6), 1289–1299.
37. Taiwo, S. F. and Kayode Ayinde (2019). Different Forms Biasing Parameter for Generalized Ridge Regression Estimator. *International Journal of Computer Applications*, 181(37), 0975 – 8887.
38. Tibshirani, R. (1996). *Regression shrinkage and selection via the LASSO*. *J. Royal. Statist. Soc B.*, Vol. 58, No. 1, p 267-288).
39. Troskie, C. G. and Chalton, D. O. (1996). A Bayesian Estimate for the Constants in Ridge Regression. *South African Statistical Journal*, 30, 119 – 137.
40. Yohai, V. J. “High breakdown point and high efficiency robust estimates for regression.” *The Annals of Statistics*, 15, 642 – 656, 1987.
41. Wold, H. (1966). *Estimation of Principle Components and Related Models by Iterative Least Squares*. In P. R. Krishnaiah (Ed.). *Multivariate Analysis*. (pp.391-420) New York, Academic Press.

APPENDIX

Table 1: AMSE of the estimators when $n = 20$ and $\sigma_{outlier}^2$ (magnitude of outliers) = 10

ESTI MAT ORS	NUMBER OF EXPLANATORY VARIABLES																	
	3									5								
	DEGREES OF MULTICOLLINEARITY									DEGREES OF MULTICOLLINEARITY								
	0.900			0.990			0.999			0.900			0.990			0.999		
	% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS		
	5%	10%	20%	5%	10%	20%	5%	10%	20%	5%	10%	20%	5%	10%	20%	5%	10%	20%
OLS	1.9	3.2	6.2	13.	32.	106	198	376	868	2.4	5.3	11.	27.		94.	241	607	153
	202	742	438	003	974	.14	.34	.55	.80	468	046	383	313	43.	141	.55	.02	2.5
	91	3	32	15	31	29	69	65	67	15	88	42	64	867	39	51	05	16
MMI	1.7	3.0	5.7	11.	30.	97.	182	347	801	2.2	4.9	10.	25.	40.	87.	224	560	141
NFA2	673	177	790	958	302	595	.42	.37	.35	634	296	563	246	878	436	.14	.47	0.8
	47	06	34	86	04	18	61	72	03	46	94	18	35	81	78	79	54	16
MMA	0.9	1.6	3.5	5.7	13.	47.	83.	161	410	1.2	2.7	6.2	11.	20.	47.	95.	284	818
XFA2	416	325	102	941	077	277	889	.37	.15	864	364	137	290	862	101	883	.61	.48
	32	72	43	25	47	22	95	86	2	47	78	82	93	21	14	04	01	64



Global Journal of Engineering Science and Research Management

MMI	1.0	1.7	3.7	5.9	13.	47.	83.	161	410	1.3	2.9	6.4	11.	21.	47.	95.	284	818
DFA2	506	775	609	635	221	821	991	.71	.63	841	379	282	349	054	422	969	.73	.73
MMF	1.6	2.6	5.4	11.	26.	82.	159	327	710	2.0	4.1	8.8	21.	36.	69.	186	437	103
A2	093	953	253	351	427	010	.61	.41	.05	385	709	682	831	899	320	.65	.69	1.2
MGM	1.4	2.4	4.8	9.0	19.	65.	106	218	504	1.9	4.0	8.5	15.	28.	57.	109	304	849
FA2	497	310	909	729	665	757	.81	.88	.25	913	857	163	423	339	475	.32	.35	.11
MHM	1.7	2.9	5.6	12.	32.	105	198	376	867	2.3	5.0	10.	27.	43.	93.	241	606	153
FA2	535	469	486	768	577	.28	.12	.14	.97	184	423	892	159	582	660	.40	.70	1.9
MMI	1.1	1.9	4.0	7.6	18.	64.	117	223	540	1.5	3.5	7.8	16.	29.	64.	151	396	104
NFA1	221	814	401	459	826	120	.22	.31	.91	801	067	248	837	041	269	.91	.43	5.0
MMA	0.8	1.4	3.2	5.6	12.	46.		161	409	1.1	2.5	5.9	11.	20.	46.	95.	284	818
XFA1	146	684	264	436	945	778	83.	.06	.69	794	025	917	237	688	811	803	.49	.25
MMI	0.8	1.4	3.2	5.6	12.	46.	83.	161	409	1.1	2.5	6.0	11.	20.	46.	95.	284	818
DFA1	221	783	437	524	953	809	800	.08	.72	866	191	073	241	700	831	808	.49	.27
MMF	0.9	1.6	3.6	6.8	15.	51.	95.	196	458	1.3	2.7	6.4	13.	24.	50.	113	308	848
A1	514	715	570	676	083	891	959	.99	.51	424	945	836	240	219	494	.16	.00	.74
MGM	0.8	1.5	3.4	5.9	13.	48.	85.	164	415	1.3	2.7	6.3	11.	21.	47.	96.	285	820
FA1	830	730	136	317	441	322	210	.71	.74	168	584	635	561	359	776	634	.75	.32
MHM	1.0	1.8	3.8	10.	28.	94.	194	369	855	1.6	3.6	8.3	25.	40.	88.	239	602	152
FA1	859	396	229	495	063	883	.78	.82	.20	754	609	022	370	436	188	.38	.34	4.1
MM	1.7	2.9	5.7	11.	30.	96.	181	344	793	2.2	4.8	10.	25.	40.	86.	222	554	138
MINF	596	985	208	895	128	778	.48	.75	.65	464	929	436	117	561	404	.88	.67	8.9
A2	34	51	6	57	87	34	3	09	17	02	38	4	06	22	39	15	1	58
MM	0.7	1.1	2.1	4.1	7.8	23.	57.	95.	190	0.9	1.8	3.0	7.4	11.	22.	64.	160	338
MAX	635	139	021	904	009	596	924	081	.42	150	079	077	559	487	783	755	.79	.06
FA2	57	97	14	65	62	61	43	6	46	36	71	07	75	36	02	68	14	6
MM	0.9	1.3	2.5	4.4	7.9	24.	58.	95.	191	1.0	2.1	3.4	7.5	11.	23.	64.	160	338
MID	002	202	416	040	936	351	048	504	.11	545	168	045	320	768	284	863	.97	.46
FA2	49	51	09	01	95	43	66	6	13	43	37	04	91	46	27	43	11	41
MM	1.5	2.6	5.2	11.	25.	76.	155	320	672	1.9	3.9	7.8	21.	35.	59.	179	388	738
MFA	817	068	565	206	564	443	.03	.96	.55	684	204	627	150	532	598	.14	.28	.80
2	29	2	5	9	59	28	92	87	57	04	41	79	3	73	13	5	97	75
MMG	1.3	2.2	4.4	8.4	16.	52.	87.	176	346	1.9	3.8	7.2	12.	23.	40.	82.	190	393
MFA	936	556	651	362	875	122	744	.11	.88	067	031	522	993	225	122	339	.28	.93
2	21	54	25	77	79	66	47	56	98	66	05	19	24	17	71	03	48	69
MMH	1.7	2.9	5.5	12.	32.	105	198	376	867	2.3		10.	27.	43.	93.	241	606	153
MFA	445	191	610	764	572	.28	.12	.14	.97	101	5.0	853	158	579	655	.40	.70	1.9
2	97	36	33	23	83	11	72	04	01	52	25	14	36	22	32	71	07	49
MM	0.9	1.6	3.0	6.5	15.	49.	101	182	408	1.3	2.9	6.0	14.	24.	51.	136	328	765
MINF	901	163	358	993	751	565	.42	.38	.38	371	733	057	853	294	359	.69	.09	.56
A1	03	75	72	28	41	53	86	1	52	8	12	89	67	06	05	69	94	67
MM	0.6	0.8	1.6	4.0	7.6	22.	57.	94.	189	0.7	1.4	2.6	7.3	11.	22.	64.	160	337
MAX	113	992	488	070	309	941	808	689	.78	696	617	231	878	244	352	656	.62	.69
FA1	65	14	83	52	63	53	84	71	7	38	77	45	07	56	73	2	53	93
MM	0.6	0.9	1.6	4.0	7.6	22.	57.		189	0.7	1.4	2.6	7.3	11.	22.	64.	160	337
MID	195	107	727	175	411	980	816	94.	.82	788	842	476	925	261	381	663	.63	.72
FA1	72	81	05	17	33	07	02	714	67	49	99	77	63	04	74	27	71	54
MM	0.7	1.1	2.3	5.5	10.	30.	73.	144	269	0.9	1.8	3.5	10.	16.	28.	87.	195	393
MFA	757	686	581	803	606	427	455	.92	.38	947	969	080	075	775	409	368	.82	.22
1	74	48	38	83	26	81	2	12	09	14	52	51	08	43	51	43	57	96
MMG	0.6	1.0	1.9	4.3	8.2	25.	59.	99.	198	0.9	1.8	3.2	7.8	12.	23.	65.	162	341
MFA	913	322	384	635	948	066	557	400	.72	581	415	840	115	230	853	701	.41	.08
1	09	58	52	51	57	35	43	87	62	58	73	2	04	08	43	83	56	8



Global Journal of Engineering Science and Research Management

MMH	0.9	1.4	2.6	10.	27.	93.	194	369	854	1.4	3.1	7.0	25.	40.	87.	239	602	152
MFA	451	308	744	196	545	636	.72	.66	.89	815	970	025	245	083	545	.36	.28	4.0
I	68	24	84	87	3	22	52	69	24	39	93	14	25	79	68	69	09	73
SMIN	1.7	3.0	5.7	11.	30.	96.	182	346	795	2.2	4.9	10.	25.	40.	86.	224	556	139
FA2	700	089	320	973	267	944	.18	.56	.15	589	056	461	241	769	585	.15	.55	1.5
	2	4	37	98	15	68	95	14	64	38	66	63	73	47	14	32	91	42
SMA	0.9	1.3	2.3	5.7	11.	27.	75.	140	227	1.1	2.1	3.5	10.	16.	27.	99.	213	418
XFA2	521	408	521	988	207	508	429	.28	.29	604	895	724	704	809	085	019	.04	.95
	96	53	87	36	73	2	88	3	81	29	21	02	22	76	02	65	67	38
SMID	1.0	1.5	2.7	5.9	11.	28.	75.	140	227	1.2	2.4	3.9	10.	17.	27.	99.	213	419
FA2	604	228	581	688	366	225	539	.64	.93	706	538	433	768	039	562	109	.20	.32
	22	208	32	44	59	14	58	86	64	92	66	42	76	66	11	06	39	02
SMF	1.6	2.6	5.2	26.	77.	158	325	679	2.0	4.0	8.0	21.	36.	61.	187	406	786	
A2	155	507	878	11.	218	453	.27	.51	.69	160	151	516	807	395	417	.62	.74	.53
	68	52	48	379	5	17	3	01	31	91	52	77	32	54	54	15	05	
SGM	1.4	2.3	4.5	9.1		54.	100	205	373	1.9	3.9	7.4	15.	26.	43.	112	237	470
FA2	584	383	419	212	18.	437	.49	.88	.49	637	110	888	169	215	340	.55	.84	.34
	39	6	82	96	839	74	23	55	08	21	81	37	5	44	59	95	43	03
SHM	1.7	2.9	5.5	12.	32.	105	198	376	867	2.3	5.0	10.	27.		93.	241	606	153
FA2	555	327	770	768	576	.28	.12	.14	.97	167	315	860	159	43.	656	.40	.70	1.9
	42	92	95	83	01	29	74	08	03	57	63	5	1	581	28	72	08	49
SMIN	1.1	1.7	3.2	7.6	17.	52.	112	210	431	1.4	3.1	6.3	16.	27.	53.	154	354	810
FA1	319	787	144	791	893	024	.01	.92	.21	960	878	440	663	083	785	.21	.60	.93
	47	51	31	42	51	66	38	03	54	8	11	89	09	84	69	7	4	17
SMA	0.8	1.1	1.9	5.6	11.	26.	75.	139	226	1.0	1.8	3.2	10.	16.	26.	98.	212	418
XFA1	334	520	292	492	069	883	327	.94	.70	465	896	096	645	607	671	936	.90	.61
	55	89	95	65	2	15	57	27	46	47	52	46	73	4	12	78	11	63
SMID	0.8	1.1	1.9	5.6	11.	26.	75.	139	226	1.0	1.9	3.2	10.	16.	26.	98.	212	418
FA1	396	623	519	579	077	920	333	.96	.74	536	096	329	649	621	699	942	.91	.64
	57	81	51	41	43	05	92	37	16	58	5	91	84	28	21	68	15	03
SMF	0.9	1.3	2.5	6.8	13.	33.	88.	180	300	1.2	2.2	4.0	12.	21.	32.	116	242	469
A1	618	885	887	867	561	968	539	.86	.86	233	657	398	830	026	377	.37	.47	.68
	39	87	79	54	99	75	02	25	86	3	55	28	4	94	05	33	26	92
SGM	0.8	1.2	2.2	5.9	11.	28.	76.	143	235	1.1	2.2	3.8	11.	17.	28.	99.	214	421
FA1	953	693	005	368	617	902	852	.95	.00	944	183	309	001	411	100	794	.45	.73
	47	32	23	37	01	65	88	78	99	46	22	27	48	94	44	39	68	4
SHM	1.0	1.6	2.8	10.	27.	93.	194	369	854	1.6	3.3	7.2	25.	40.	87.	239	602	152
FA1	948	102	792	523	905	875	.76	.76	.94	139	821	353	341	289	652	.38	.30	4.0
	51	6	26	18	59	26	75	73	97	96	31	74	85	5	04	69	26	83
LTSM	1.7	3.0		12.	30.	97.	183	350	802	2.2	4.9	10.	25.	41.	87.	227	566	141
INFA	876	399		109	581	987	.95	.63	.43	953	767	611	603	374	850	.31	.71	4.7
2	24	86	847	72	17	47	39	62	13	54	96	34	48	33	77	18	55	2
LTSM	1.1	1.8	3.2	7.5	16.	46.	105	204	391	1.6	3.2	6.2	16.	26.		147	360	794
AXFA	779	262	934	462	536	776	.69	.23	.26	196	740	058	064	151	49.	.74	.77	.07
2	56	82	13	74	68	47	76	96	97	19	44	89	77	6	795	4	89	41
LTSM	1.2	1.9	3.5	7.6	16.	47.	105	204	391	1.6	3.4	6.4	16.	26.	50.	147	360	794
IDFA	548	525	723	714	656	311	.77	.50	.75	827	277	246	104	298	106	.80	.87	.30
2	66	69	27	84	85	57	31	07	64	56	01	02	15	94	28	01	35	94
LTSM	1.6	2.7	5.4	11.	27.	82.	164	334	710	2.1	4.3	8.9	23.	38.	71.	202	473	101
FA2	640	597	218	639	415	763	.97	.31	.78	299	698	520	175	365	171	.73	.65	7.8
	43	6	89	92	82	58	46	29	77	23	29	85	12	51	74	97	79	34
LTSG	1.5	2.5	4.8	9.9	22.	65.	122	249	492	2.0	4.3	8.5	18.	31.	60.	156	375	825
MFA	442	294	481	561	028	985	.80	.35	.69	963	036	923	850	957	051	.24	.71	.44
2	24	38	38	42	5	05	75	71	84	12	48	2	91	84	23	02	53	85
LTSH	1.7	2.9	5.6	12.	32.	105	198	376	867	2.3	5.0	10.	27.	43.	93.	241	606	153
MFA	760	783	576	780	587	.30	.12	.14	.97	379	718	920	164	592	668	.40	.70	1.9
2	17	03	05	86	44	11	82	26	21	68	05	22	04	55	58	79	19	5
LTSM	1.3	2.1	3.8	8.9	21.	64.	130	252	532	1.8	3.8	7.8	19.	32.	66.	181	443	103
INFA	059	327	896	128	352	261	.93	.81	.40	128	595	766	801	491	487	.93	.68	2.8
1	39	4	32	89	28	23	07	25	41	25	64	76	24	32	79	7	85	85
LTSM	1.0	1.6	3.0	7.4	16.	46.	105	203	390	1.5	3.0	5.9	16.	26.	49.	147	360	793
AXFA	944	913	016	356	430	295	.62	.99	.81	535	991	910	029	020	519	.69	.69	.85
1	44	64	62	69	05	61	72	61	56	74	55	98	19	46	74	19	12	68



Global Journal of Engineering Science and Research Management

LTSM	1.0	1.6	3.0	7.4	16.	46.	105	204	390	1.5	3.1	6.0	16.	26.	49.	147	360	793
IDFA	986	988	176	420	436	324	.63	.01	.84	577	108	051	031	029	538	.69	.69	.87
1	75	6	85	52	41	55	15	11	.38	97	13	51	69	5	66	56	74	22
LTSM	1.1	1.8	3.4	8.3	18.	51.	114	232	442	1.6	3.3		17.	28.	53.	158	378	825
FAI	847	599	556	403	255	438	.55	.22	.97	556	183	6.4	381	776	166	.61	.48	.05
1	94	06	8	19	37	41	7	98	29	44	71	817	02	53	8	43	48	67
LTSG	1.1	1.7	3.1	7.6	16.	47.	106	206	397	1.6	3.2	6.3	16.	26.	50.	148	361	795
MFA	377	756	895	479	843	808	.66	.84	.01	391	907	582	246	535	453	.23	.62	.84
1	12	3	33	56	48	54	79	25	53	11	96	04	81	1	38	13	89	54
LTSH	1.2	2.0	3.6	10.	28.	95.	194	370	855	1.8	3.9	8.4	25.	40.	88.	239	602	152
MFA	799	121	677	964	653	379	.91	.10	.34	817	791	192	669	954	537	.48	.48	4.2
1	37	1	78	27	19	99	89	64	04	39	98	8	02	65	97	86	66	53
LMS	1.8	3.0	5.8	12.	30.	98.	185	353	808	2.3	5.1	10.	26.	42.	90.	233	580	146
MINF	030	612	383	226	779	947	.72	.90	.96	554	075	867	318	314	316	.02	.72	0.7
A2	22	12	49	73	53	7	06	45	99	27	73	5	55	39	43	49	84	53
LMS		2.0	3.8	8.6	19.	59.	124	237	479	2.0	4.3	8.5	22.	35.	72.	195	472	117
MAX	1.3	105	918	211	595	558	.00	.63	.75	180	190	334	130	213	306	.91	.00	5.3
FA2	329	26	87	9	85	99	41	89	19	67	67	34	48	77	56	27	46	87
LMS	1.3	2.1	4.1	8.7	19.	59.	124	237	480	2.0	4.3	8.6	22.	35.	72.	195	472	117
MID	892	179	110	219	689	968	.06	.84	.13	506	899	441	148	275	449	.93	.05	5.5
FA2	39	94	38	68	4	31	33	29	96	67	62	45	74	19	61	54	43	07
LMS	1.7	2.8	5.5	11.	28.	86.	170	340	732	2.2	4.8	9.9	25.	40.	82.	220	529	127
MFA	026	162	430	845	098	715	.31	.52	.22	723	194	525	219	764	158	.69	.88	9.0
2	57	98	95	92	8	21	55	31	09	46	62	98	94	05	41	6	21	63
LMS	1.6	2.6	5.0	10.	23.	73.	137	272	558	2.2	4.7	9.7	23.	37.	77.	199	479	119
GMF	086	158	931	512	809	942	.40	.68	.42	558	893	623	377	732	017	.45	.40	1.0
A2	3	99	06	21	3	62	11	57	95	33	54	24	72	47	57	24	11	26
LMS	1.7	3.0	5.7	12.	32.	105	198	376	867	2.3	5.1	11.	27.	43.	93.	241	606	153
HMF	941	086	273	794	598	.32	.12	.14	.97	779	534	047	188	640	744	.41	.71	1.9
A2	11	25	69	66	51	96	98	59	62	65	76	89	61	69	07	51	43	63
LMS	1.4	2.2	4.3	9.6	23.	72.	143	275	589	2.1	4.5	9.3	23.	37.	79.	210	514	128
MINF	271	725	565	946	286	654	.69	.39	.48	162	880	878	785	974	983	.87	.13	5.5
A1	89	09	98	49	24	44	21	87	69	86	64	42	02	85	18	72	02	98
LMS	1.2	1.8	3.6	8.5	19.	59.	123	237	479	1.9	4.2	8.4	22.	35.	72.	195	471	117
MAX	723	963	555	296	512	189	.94	.44	.38	835	394	232	113	159	180	.89	.95	5.2
FA1	16	05	46	65	18	99	87	87	9	28	23	67	97	16	45	17	85	75
LMS	1.2	1.9	3.6	8.5	19.	59.	123	237	479	1.9	4.2	8.4	22.	35.	72.	195	471	117
MID	754	026	688	350	517	212	.95	.46	.41	856	446	305	115	162	189	.89	.96	5.2
FA1	25	78	92	51	2	24	22	03	16	95	34	96	13	91	08	31	17	83
LMS	1.3	2.0	4.0	9.2	20.	63.	130	259	519	2.0	4.3	8.6	22.	36.	73.	200	480	119
MFA	378	390	198	474	913	091	.97	.31	.83	367	394	730	731	325	857	.46	.76	0.8
1	68	65	88	52	99	17	76	11	85	38	85	11	54	29	54	72	79	34
LMS	1.3	1.9	3.8	8.7	19.	60.	124	239	484	2.0	4.3	8.6	22.	35.	72.	196	472	117
GMF	037	676	089	031	833	347	.76	.66	.28	281	267	105	214	373	609	.11	.44	6.2
A1	93	31	41	69	75	37	83	48	67	93	78	76	77	73	31	05	57	89
LMS	1.4	2.1	4.1	11.	29.	96.	195	370	855	2.1	4.6	9.6	26.	42.	90.	239	603	152
HMF	119	753	635	298	146	748	.11	.48	.89	477	293	626	320	072	548	.94	.28	5.4
A1	47	45	02	72	11	21	85	93	58	56	67	51	85	5	59	11	1	02
LAD	1.7	2.9	5.7	11.	30.	96.	180	343	791	2.2	4.8	10.	25.	40.	86.	222	552	138
MINF	546	902	024	858	046	464	.99	.74	.25	397	779	415	059	461	218	.40	.83	5.6
A2	74	48	94	05	71	47	31	93	27	4	73	05	65	92	05	78	73	9
LAD	0.6	0.7	1.4	2.7	4.2	11.	43.	55.	92.	0.7	1.3	2.2	5.4	7.6	14.	46.	105	248
MAX	227	920	894	683	882	060	982	676	944	479	695	549	887	787	426	807	.01	.95
FA2	83	55	34	77	32	26	82	92	77	79	1	1	09	48	29	86	79	5
LAD	0.7	1.0	2.0	3.0	4.4	11.	44.	56.	93.	0.9	1.7	2.7	5.5	7.9	14.	46.	105	249
MID	836	482	281	309	928	894	109	125	624	086	374	089	675	855	972	921	.20	.37
FA2	68	61	39	13	1	74	2	78	72	62	92	1	45	78	03	97	91	12
LAD	1.5	2.5	5.2	11.	25.	73.	152	318	658	1.9	3.8	7.6	20.	35.	56.	175	367	690
MFA	630	649	003	113	070	941	.51	.17	.96	395	098	688	809	055	875	.34	.39	.86
2	59	11	9	87	76	97	27	13	98	65	02	12	98	78	28	45	34	39
LAD	1.3	2.1	4.3	7.9	14.	45.	77.	151	276	1.8	3.6	7.0	11.	21.	34.	66.	138	311
GMF	538	671	117	446	950	316	114	.22	.20	717	779	032	708	223	605	417	.43	.52
A2	46	3	12	01	39	61	73	2	64	27	43	14	5	58	29	68	15	43



Global Journal of Engineering Science and Research Management

LAD	1.7	2.9	5.5	12.	32.	105	198	376	867	2.3	5.0	10.	27.	43.	93.	241	606	153
HMF	380	021	271	762	570	.27	.12	.14	.96	067	184	845	158	578	654	.40	.70	1.9
A2	61	02	19	18	98	82	71	02	98	11	24	86	03	37	55	71	06	49
LAD	0.8	1.4	2.6	5.7	13.	42.	92.	158	350	1.2	2.7	5.6	13.	22.	47.	127	297	719
MINF	891	108	284	360	605	239	579	.69	.23	320	343	323	812	449	511	.96	.92	.85
A1	5	46	52	5	09	95	58	22	38	35	51	13	2	68	77	41	22	38
LAD	0.4	0.5	0.9	2.5	4.1	10.	43.	55.	92.	0.5	0.9	1.8	5.4	7.4	13.	46.	104	248
MAX	485	277	388	458	131	368	865	259	307	836	558	224	191	203	980	702	.84	.57
FA1	75	15	53	26	26	42	66	27	07	73	05	09	38	99	54	58	16	23
LAD	0.4	0.5	0.9	2.5	4.1	10.	43.	55.	92.	0.5	0.9	1.8	5.4	7.4	14.	46.	104	248
MID	572	413	669	583	233	408	872	285	348	935	819	489	239	376	009	710	.85	.59
FA1	45	15	17	8	96	84	92	62	65	15	63	87	62	7	65	07	41	95
LAD	0.6	0.8	1.8	4.4	7.4	19.	61.	113	183	0.8	1.4	2.8	8.3	13.	20.	72.	144	310
MFA	371	601	036	860	711	082	017	.92	.17	397	760	272	948	752	929	116	.81	.72
1	43	38	01	39	05	35	97	24	13	91	3	88	82	88	52	37	82	34
LAD	0.5	0.6	1.2	2.9	4.8	12.	45.	60.	101	0.7	1.4	2.5	5.8		15.	47.	106	252
GMF	383	902	887	810	206	709	679	373	.51	976	097	710	643	8.5	610	817	.76	.15
A1	29	45	43	29	75	95	71	33	36	67	8	46	16	002	93	77	5	59
LAD	0.8	1.1	2.1	9.9	27.	93.	194	369	854	1.3	2.9	6.7	25.	39.	87.	239	602	152
HMF	346	616	659	820	281	121	.70	.61	.80	963	876	086	201	969	417	.35	.26	4.0
A1	15	32	77	39	7	58	06	87	31	49	03	67	39	68	91	95	56	59

Table 2: AMSE of the estimators when $n = 20$ and $\sigma_{outlier}^2$ (magnitude of outliers) = 100

ESTI MAT ORS	NUMBER OF EXPLANATORY VARIABLES																	
	3									5								
	DEGREES OF MULTICOLLINEARITY									DEGREES OF MULTICOLLINEARITY								
	0.900			0.990			0.999			0.900			0.990			0.999		
	% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS		
5%	10	20	5%	10	20	5%	10	20	5%	10	20	5%	10	20	5%	10	20	
OLS	153	244	581	192	293	824	136	539	625	147	484	783	243	623	932	262	414	128
	.60	.90	.73	2.8	3.5	1.7	85.	77.	46.	.33	.03	.18	9.7	6.4	1.5	51.	82.	763
	74	34	56	09	04	48	45	96	14	86	91	69	11	29	65	26	69	.1
MMI	141	225	536	176	269	757	125	497	574	135	449	728	224	576	868	242	383	119
NFA2	.06	.81	.71	5.4	6.7	6.3	69.	79.	44.	.48	.06	.40	3.3	1.0	0.3	12.	45.	289
	84	29	3	65	65	16	93	6	71	21	46	52	19	31	97	73	6	.3
MMA	67.	121	321	620	109	354	442	255	272	62.	217	414	840	261	465	107	169	638
XFA2	272	.18	.80	.16	7.3	4.2	5.6	91.	74.	554	.93	.41	.17	2.3	8.1	79.	41.	63.
	8	13	47	38	34	45	01	72	96	06	72	47	58	48	04	48	65	05
MMI	79.	135	349	639	112	360	443	256	273	67.	235	440	847	262	468	107	169	638
DFA2	684	.69	.63	.13	7.7	8.3	9.7	17.	46.	643	.53	.50	.67	8.0	3.6	90.	51.	96.
	67	78	24	54	69	23	88	54	84	35	28	16	22	63	07	14	57	11
MMF	122	214	510	156	708	102	409	553	123	380	658	169	446	183	309	964		
A2	.7	.41	.19	6.2	241	9.4	01.	67.	69.	.75	.09	.58	3.1	0.9	770	35.	23.	62.
	61	66	17	5.1	57	96	41	32	75	31	75	62	46	3.7	01	23	85	
MGM	112	190	458	115	185	546	657	305	375	119	368	631	119	331	591	119	189	680
FA2	.95	.14	.20	7.4	5.8	5.3	6.2	75.	58.	.36	.95	.05	5.1	4.9	6.4	54.	55.	91.
	01	41	25	74	77	35	75	92	98	78	28	44	35	37	36	12	36	65
MHM	137	216	523	190	289	816	136	539	624	135	460	738	242	621	927	262	414	128
FA2	.87	.48	.46	4.5	6.5	6.8	68.	35.	70.	.79	.46	.20	5.6	1.2	0.3	38.	55.	707
	09	75	49	56	41	7	22	93	31	61	72	88	27	73	23	39	18	.6
MMI	81.	143	365	101	162	480	747	339	366	86.	302	521	141	390	627	164	261	865
NFA1	595	.75	.55	8.2	8.8	4.1	6.5	34.	23.	060	.61	.76	7.7	3.1	8.3	47.	39.	34.
	62	89	86	79	33	83	93	7	61	54	61	67	53	6	83	8	32	41
MMA	51.	104	289	603	107	348	441	255	272	57.	199	386	833	259	463	107	169	638
XFA1	054	.61	.64	.25	0.3	5.8	2.4	67.	06.	742	.78	.96	.51	8.1	4.9	69.	32.	32.
	84	32	61	54	19	03	83	57	54	31	64	77	11	92	34	65	42	09
MMI	52.	105	291	604	107	348	441	255	272	58.	200	388	833	259	463	107	169	638
DFA1	015	.55	.56	.26	1.9	9.5	3.2	69.	11.	051	.99	.85	.97	9.1	6.5	70.	33.	34.
	26	61	32	83	3	23	96	08	12	78	97	13	22	82	89	35	08	34
MMF	61.	128	334	778	130	421	530	276	337	71.	231	442	963	288	523	120	194	692
A1	934	.20	.88	.75	8.8	4.8	3.4	77.	54.	290	.07	.79	.79	0.8	5.0	23.	30.	17.
	97	66	65	93	69	14	02	4	47	48	99	4	49	81	29	9	46	54



Global Journal of Engineering Science and Research Management

MGM	57.	114	308	647	113	455	259	278	68.	226	427	862	265	473	108	170	641	
FAI	876	.26	.52	.78	3.1	364	7.2	03.	44.	399	.11	.70	.65	6.3	9.4	43.	59.	02.
MHM	74.	129	345	167	247	727	134	532	613	85.	324	530	225	590	869	260	410	127
FAI	100	.24	.13	5.4	5.0	0.5	03.	93.	21.	408	.05	.30	6.7	5.6	6.0	62.	80.	949
MM	61	76	92	44	85	72	23	51	23	95	96	71	53	59	47	63	09	.4
MM	140	224	531	176	268	751	125	491	568	134	446	720	223	570	857	240	380	
MINF	.67	.12	.15	0.2	1.7	0.4	15.	70.	39.	.71	.18	.10	4.2	9.0	0.8	51.	07.	117
A2	54	09	82	51	91	03	07	43	41	39	5	7	59	47	62	8	44	563
MM	58.	84.	171	473	606	127	263	115	106	42.	138	184	592	136	165	686	811	204
MAX	010	535	.01	.64	.85	9.5	2.8	24.	95.	073	.68	.02	.55	5.6	5.9	2.0	3.0	41.
FA2	13	33	01	68	45	24	24	36	42	55	52	57	14	11	32	51	7	93
MM	72.	105	224	493	646	137	264	115	108		164	234	601	138	169	687	812	204
MID	296	.00	.32	.90	.99	8.4	9.0	57.	00.	49.	.06	.71	.47	6.5	8.3	4.4	5.6	95.
FA2	74	29	86	51	07	49	22	52	02	169	83	9	59	5	63	47	47	45
MM	120	210	496	154	235	690	978	366	542	121	362	621	161	400	714	168	282	816
MFA	.84	.56	.42	5.1	4.0	0.2	1.1	46.	31.	.23	.10	.55	2.2	1.2	6.5	25.	88.	79.
2	2	1	74	26	8	4	49	63	14	2	23	72	23	4	79	22	7	2
MMG	110	179	418	108	164	450	528	195	275	116	347	578	102	237	403	836	110	285
MFA	.03	.78	.67	5.9	2.8	3.6	5.7	28.	96.	.00	.74	.41	2.8	1.3	3.0	5.7	30.	19.
2	87	54	93	42	7	07	39	83	2	34	48	55	02	68	43	5	12	82
MMH	137	213	514	190	289	816	136	539	624	135	459	733	242	621	926	262	414	128
MFA	.27	.35	.49	4.4	6.0	5.9	68.	35.	70.	.04	.20	.03	5.5	1.1	9.6	38.	55.	707
2	54	71	1	88	92	32	21	85	16	84	95	32	72	1	73	38	15	.6
MM	74.	116	254	926	133	340	641	251	260	74.	258	389	128	321	470	143	215	637
MINF	490	.36	.69	.30	7.2	8.8	4.7	78.	55.	000	.90	.17	8.5	4.3	2.5	51.	10.	64.
A1	63	9	45	07	55	52	94	81	51	69	77	64	98	38	31	62	83	46
MM	39.	62.	113	456	572	119	261	114	105	35.	113	133	584	134	161	685	810	203
MAX	312	077	.37	.34	.88	5.7	7.9	93.	98.	343	.35	.33	.72	7.3	9.4	0.6	1.4	92.
FA1	11	15	11	43	8	29	58	88	5	01	53	56	91	39	43	83	52	67
MM	40.	63.	116	457	574	120	261	114	106	35.	114	136	585	134	162	685	810	203
MID	429	261	.34	.34	.82	0.6	8.8	95.	04.	768	.93	.45	.26	8.5	1.9	1.4	2.2	96.
FA1	01	42	48	71	82	02	76	76	59	75	79	09	53	9	23	88	78	17
MM	51.	94.	196	650	896	240	369	147	212	54.	157	239	742	174	273	845	117	307
MFA	859	423	.03	.90	.02	0.4	8.1	32.	86.	189	.64	.17	.63	5.7	5.3	8.0	36.	49.
1	36	74	18	62	33	76	71	72	43	27	13	53	14	76	87	29	44	83
MMG	47.	74.	146	503	654	143	278	119	115	50.	150	209	619	142	179	693	826	208
MFA	185	902	.05	.31	.17	1.0	6.3	51.	50.	214	.47	.81	.51	5.3	5.8	7.6	6.6	40.
1	79	78	82	8	25	98	91	33	73	77	58	73	7	16	58	87	34	94
MMH	65.	96.	217	166	242	713	133	532	612	72.	287	406	224	588	861	260	410	127
MFA	791	422	.54	5.3	4.8	2.5	99.	74.	83.	344	.71	.31	9.4	3.7	0.7	60.	74.	936
1	68	48	53	14	91	59	98	86	8	02	54	16	74	21	48	62	68	.4
SMIN	141	224	531	177	269	752	125	494	569	135	448		224	573	858	242	381	117
FA2	.40	.83	.98	0.9	2.7	7.9	83.	70.	61.	.39	.05	721	3.0	1.0	7.6	09.	77.	878
5	76	5	51	57	38	87	79	36	9	64	.51	67	5	23	78	16	.7	
SMA	75.	103	203	764	947	201	477	199	146	60.	189	231	828	201	221	109	128	294
XFA2	032	.68	.50	.12	.07	3.5	7.8	01.	67.	339	.88	.95	.94	1.7	3.5	00.	80.	95.
56	82	19	62	64	86	32	23	42	06	69	08	88	74	98	81	19	81	
SMID	86.	120	250	780	980	210	479	199	147	65.	210	277	836	202	225	109	128	295
FA2	086	.79	.64	.09	.98	2.9	1.0	30.	68.	807	.55	.75	.37	9.6	4.3	11.	91.	46.
49	21	32	65	6	36	54	57	53	72	41	69	9	11	41	18	53	46	
SMF	124	212	498	158	239	695	102	390	544	123	374	628	168	421	723	184		846
A2	.35	.26	.61	7.5	7.8	2.9	76.	70.	64.	.52	.06	.62	7.2	8.4	8.3	52.	296	26.
87	13	17	64	37	2	61	59	5	55	27	68	55	47	34	52	55	18	
SGM	115	184	425	122	179	480	679	260	299	119	361	588	118	284	437	120	153	367
FA2	.55	.65	.70	5.3	1.8	2.1	7.8	02.	54.	.07	.85	.76	3.5	4.8	5.2	75.	03.	55.
82	52	4	88	16	02	5	95	5	49	22	37	59	26	95	23	56	92	2
SHM	138	214	516	190	289	816	136	539	624	135	460	733	242	621	926	262	414	128
FA2	.25	.85	.00	4.6	6.4	6.1	68.	35.	70.	.67	.01	.79	5.6	1.1	9.7	38.	55.	707
97	74	09	65	17	46	22	89.	19	28	09	67	31	74	6	38	17	.6	
SMIN	87.	130	277	110	154	385	765	302	285	85.	287	416	140	354	498	165	239	683
FA1	776	.31	.54	4.6	0.2	4.4	3.5	54.	69.	072	.87	.84	8.1	9.8	3.7	91.	56.	67.
35	22	79	36	63	05	02	97	63	14	63	65	05	88	98	01	22	32	



Global Journal of Engineering Science and Research Management

SMA	60.	84.	151	749	916	193	476	198	145	55.	168	185	822	199	217	108	128	294
XFAI	078	443	.36	.96	.98	5.7	5.5	73.	72.	094	.86	.40	.36	5.9	7.9	91.	69.	49.
	31	83	69	09	55	47	91	87	85	18	47	19	78	41	06	25	69	04
SMID	61.	85.	154	750	918	194	476	198	145	55.	170	188	822	199	218	108	128	294
FAI	001	517	.20	.81	.77	0.3	6.3	75.	78.	431	.22	.34	.82	7.0	0.3	91.	70.	52.
	23	32	73	47	82	69	51	58	89	82	25	67	2	36	59	93	44	37
SMF	70.	111	225	898	118	298	559	223	242	69.		281	952	232	320	121	158	387
AI	206	.95	.63	.88	3.1	9.4	8.4	96.	91.	677	205	.77	.02	7.0	2.2	46.	81.	37.
	36	44	09	15	5	69	16	99	19	73	.33	45	55	29	12	02	16	08
SGM	66.	95.	181	787	986	214	490	202	154	66.	199	255	851	206	234	109	130	298
FAI	488	584	.31	.40	.95	9.8	0.5	60.	80.	613	.50	.28	.27	2.1	6.2	63.	16.	70.
	42	66	26	55	9	55	46	78	91	41	07	58	29	85	31	45	43	05
SHM	80.	113	245	168	246	716	134	532	612	83.	311	430	225	589	862	260	410	127
FAI	417	.73	.01	7.3	0.6	9.2	0.4	82.	90.	736	.12	.53	7.1	3.6	3.4	61.	77.	938
		33	99	86	59	66	85	8	78	12	4	09	75	77	16	95	63	.3
LTSM	142	227	537	178	272	759	127	502	575	137	455	729	227	582	869	246	387	
INFA	.68	.57	.44	9.5	0.0	8.6	20.	06.	32.	.68	.39	.32	6.5	7.3	1.4	09.	41.	119
2	03	96	91	03	44	75	84	75	34	11	68	06	83	21	78	03	85	311
LTSM	92.		315	103		362	691	305	276	92.	298	408	137	354	455	159	224	587
AXFA	712	144	.25	3.9	143	8.7	2.8	91.	04.	213	.35	.46	0.2	3.7	6.4	78.	56.	61.
2	54	.36	44	61	9.1	77	37	12	71	87	49	88	4	95	89	79	84	33
LTSM	100		344	104	146	369	692	306		95.	310	435	137	355	458	159	224	587
IDFA	.73	155	.73	4.8	3.9	2.6	1.9	12.	276	266	.54	.93	4.5	4.7	2.4	85.	64.	97.
2	88	.46	98	45	59	85	2	1	76	18	35	93	12	1	42	58	01	16
LTSM	129	217	511	164	248	713	109	430	554	129	407	660	189	484	770	207	328	950
FA2	.12	.91	.12	2.3	6.9	3.1	19.	45.	89.	.55	.16	.08	2.5	9.4	4.3	46.	46.	35.
	26	93	03	54	76	57	51	23	71	47	53	59	47	99	22	39	43	91
LTSG	122	198	458	136	204	555	833	346	378	126	399	632	157	403	586	167	239	635
MFA	.44	.09	.43	5.1	2.1	3.8	8.4	48.	38.	.67	.70	.45	5.7	7.6	1.7	23.	19.	02.
2	16	84	5	75	47	32	51	5	87	61	75	12	58	51	98	21	5	16
LTSH	140	219	524	190	289	816	136	539	624	137	463	739	242	621	927	262	414	128
MFA	.03	.70	.58	5.2	7.5	7.3	68.	36.	70.	.86	.68	.05	6.0	1.7	0.7	38.	55.	707
2	73	28	25	53	9	81	3	04	47	52	93	26	49	46	16	44	29	.7
LTSM	101	161	361	127	186	489	896	373	369	106	355	520	171	445	623	195	292	840
INFA	.96	.67	.61	5.4	3.1	6.4	3.2	78.	08.	.20	.75	.84	3.9	1.2	6.6	60.	13.	75.
1	8	14	59	42	75	46	09	16	27	73	02	41	72	76	43	53	03	56
LTSM	81.	131	281	102	141	357	690	305	275	89.	285	380	136	353	453	159	224	587
AXFA	852	.92	.74	4.2	6.7	1.8	4.0	71.	37.	298	.77	.09	6.3	4.0	3.2	72.	50.	28.
1	64	35	3	31	97	29	29	48	97	92	14	04	87	38	52	51	17	14
LTSM	82.	132	283	102	141	357	690	305	275	89.	286	381	136	353	453	159	224	587
IDFA	522	.61	.66	4.8	8.1	5.2	4.9	72.	42.	486	.59	.94	6.6	4.7	4.8	72.	50.	30.
1	31	98	64	25	36	57	51	71	2	93	56	7	56	15	7	96	65	5
LTSM	89.	149	329	112		430	748	322	340	97.	307	438	143	373	515	167	242	647
FA1	209	.71	.10	6.9	160	4.2	1.6	88.	52.	439	.47	.35	9.8	2.8	4.1	67.	65.	70.
	63	67	49	33	9.6	69	09	12	75	17	26	22	18	25	48	37	45	05
LTSG	86.	139	301	104	146	372	699	308	281	95.	304	422	138	357	463	160	225	590
MFA	509	.11	.25	9.8	8.3	5.8	7.1	44.	70.	717	.03	.46	2.9	4.5	9.6	19.	42.	22.
1	24	99	71	24	17	39	6	42	91	64	88	16	57	05	89	62	3	88
LTSH	96.	150	340	172	253	729	134	533	613	105	367	529	228	594	871	260	410	127
MFA	442	.60	.69	1.8	2.7	8.4	18.	13.	36.	.55	.16	.30	7.3	1.6	0.5	70.	95.	955
1	2	75	95	19	54	75	89	71	56	44	25	69	21	89	41	57	93	.1
LMS	143	229	541	180	274	765	128	507	579	141	464	741	233	597	887	252		121
MINF	.96	.60	.51	7.4	6.3	6.9	48.	41.	32.	.32	.67	.91	0.1	0.9	3.2	06.	397	945
A2	25	59	09	04	98	3	34	45	73	14	94	26	34	15	7	18	47	.2
LMS	104	164	349	121	180	448	854	355	337	117	381	552	187	487	658	211	322	894
MAX	.64	.71	.62	0.7	5.8	1.3	5.7	80.	34.	.51	.30	.16	3.6	9.6	5.7	07.	35.	76.
FA2	36	77	33	1	78	18	41	82	92	89	06	42	54	74	33	64	36	69
LMS	110	173	375	121	182	453	855	355	337	119	387	567	187	488	659	211	322	894
MID	.73	.11	.08	9.3	3.3	2.4	2.5	96.	88.	.03	.14	.11	5.4	4.5	9.6	10.	38.	94.
FA2	02	36	44	35	42	16	4	67	41	79	91	26	66	47	76	72	27	32
LMS	132	221	518	168	256	726	114	450	561	136	437	696	212	548	828	232	368	108
MFA	.88	.63	.67	8.7	2.3	2.7	59.	92.	60.	.90	.31	.72	4.2	6.1	2.9	54.	94.	003
2	14	46	81	44	81	36	23	97	79	61	79	35	92	28	67	87	51	.7



Global Journal of Engineering Science and Research Management

LMS	127	205	473	147	223	599	958	386	417	135	433	679	196	510	727	214	328	917
GMF	.57	.84	.31	0.9	1.7	1.9	7.3	62.	47.	.36	.26	.71	7.0	5.1	1.0	36.	78.	89.
A2	25	13	89	17	95	45	23	08	12	8	24	13	83	25	41	19	6	6
LMS	141	223	530	190	289	816	136	539	624	141	469	749	242	621	927	262	414	128
HMF	.83	.13	.06	6.1	9.0	9.1	68.	36.	70.	.40	.87	.08	7.7	4.2	5.8	38.	56.	708
A2	59	09	37	46	92	87	45	33	76	74	46	86	62	62	52	93	22	.5
LMS	111	177	389	140	210	547	100	407		124	409	614	203	529	747	227	352	102
MINF	.67	.82	.69	0.7	3.4	6.5	36.	40.	410	.60	.95	.40	4.4	8.6	1.7	08.	52.	240
A1	02	41	74	67	98	41	53	49	09	58	58	1	56	04	16	19	69	.5
LMS	96.	155	321	120	179	443	853	355	336	116	375	536	187	487	657	211	322	894
MAX	611	.32	.27	2.9	0.0	5.3	9.4	65.	84.	.06	.35	.76	2.0	5.3	3.0	04.	32.	60.
FA1	46	94	69	82	08	91	35	98	83	47	75	95	27	11	71	79	67	35
LMS	97.	155	322	120	179	443	853	355	336		375	537	187	487	657	211	322	894
MID	099	.85	.85	3.4	0.9	8.1	9.8	66.	88.	116	.75	.79	2.1	5.6	3.9	04.	32.	61.
FA1	46	13	1	61	8	74	29	91	04	.16	47	47	4	14	59	99	86	52
LMS	102	168	361	128	192	501	896	368	387	120	385	568	190	496	689	214	330	924
MFA	.02	.76	.56	4.2	4.9	3.7	5.9	68.	51.	.12	.66	.43	4.0	4.6	7.9	55.	34.	14.
1	25	69	36	28	5	57	88	36	74	81	09	36	13	6	39	63	05	44
LMS	100	160	337	122	182	455	860	357	341	119	384	559	187	489		211	322	896
GMF	.02	.75	.63	3.2	6.3	8.8	8.6	72.	63.	.26	.00	.75	9.0	3.3	663	26.	70.	05.
A1	11	86	41	81	93	04	81	51	02	37	86	8	71	83	0	09	51	06
LMS	107	169	371	175	259	739	134	533	613	124	417	620	233	603	888	261	411	128
HMF	.61	.49	.42	0.6	8.1	7.7	35.	52.	77.	.52	.32	.90	7.5	3.9	4.5	02.	62.	035
A1	39	15	04	12	64	92	38	33	01	98	52	72	94	27	21	62	44	.3
LAD	139	222	529	175	266	748	124	488	566	133	443	717	222	567	853	238	378	117
MINF	.98	.91	.00	0.2	9.8	6.7	56.	74.	12.	.84	.59	.49	0.2	6.6	6.0	28.	15.	069
A2	65	82	12	2	13	23	27	28	36	22	86	55	43	92	88	98	94	.4
LAD	28.	31.	71.	20.	27.	59.	55.	134	44.	7.7	29.	57.	11.	20.	132	185	68.	137
MAX	802	117	215	029	211	050	880	.99	741	619	490	003	947	160	.37	.85	554	.19
FA2	3	79	8	65	73	04	32	59	57	06	58	87	01	1	57	73	2	52
LAD	50.	62.	143	38.	62.	129	61.	146	68.	17.	63.	119	18.	32.	155	191	71.	148
MID	195	021	.92	685	863	.04	975	.61	888	255	834	.22	108	190	.14	.37	494	.92
FA2	43	99	54	9	59	98	03	54	88	3	97	21	53	48	68	24	93	19
LAD	116	207	490	149	229	682	922	334	537	117	340	606	142	352	689	141	260	746
MFA	.74	.39	.61	5.7	5.4	4.2	5.4	73.	57.	.88	.83	.50	6.8	8.7	7.3	96.	57.	07.
2	81	5	24	09	34	35	04	72	97	54	94	79	31	21	41	44	05	23
LAD	103	169	399	877	138	398	325	977	205	111	321	555	578	123	294	200	317	791
GMF	.02	.12	.17	.58	9.9	5.7	7.3	7.1	29.	.34	.93	.36	.53	5.1	4.6	2.8	5.6	1.1
A2	94	86	02	7	28	26	28	47	2	12	94	09	3	01	34	19	43	21
LAD	135	210	509	190	289	816	136	539	624	134	458	731	242	621	926	262	414	128
HMF	.92	.17	.97	4.3	5.8	5.6	68.	35.	70.	.27	.19	.56	5.5	1.0	9.5	38.	55.	707
A2	81	85	48	45	16	58	19	83	12	51	75	53	09	41	39	37	14	.6
LAD	53.	79.	185	646	973	259	478	176	184	53.	199	318	964	242	381	105	170	517
MINF	438	237	.60	.27	.66	3.9	4.6	59.	46.	399	.14	.39	.36	5.1	3.5	81.	66.	24.
A1	03	48	24	12	82	5	86	56	64	78	07	07	35	02	33	86	93	14
LAD	2.2	2.0	3.3	8.2	5.8	18.	50.	123	20.	0.9	1.9	6.6	8.1	13.	118	180	65.	125
MAX	766	048	891	319	760	767	236	.06	944	915	860	889	219	086	.87	.77	639	.71
FA1	75	22	15	62	3	73	4	01	65	69	8	06	96	66	85	13	32	58
LAD	3.6	3.1	6.2	9.0	7.3	22.	50.	124	24.	1.2	3.1	8.8	8.3	13.	119	181	65.	127
MID	120	965	953	770	608	156	879	.58	804	552	388	520	948	587	.99	.28	975	.20
FA1	82	31	51	5	83	68	66	96	2	74	45	12	59	54	31	19	19	48
LAD	19.	45.	105	243	368	129	117	347	119	24.	54.	124	186	414	128	213	408	105
MFA	588	948	.06	.69	.52	8.6	8.3	6.3	99.	405	921	.86	.17	.49	7.4	0.8	1.1	26.
1	27	35	61	16	49	89	17	83	17	82	36	46	39	29	63	93	77	02
LAD	12.	17.	38.	48.	70.	174	151	393	438	18.	45.	88.	34.	61.	228	228	127	272
GMF	735	306	973	688	100	.14	.20	.86	.77	726	122	092	484	964	.25	.95	.98	.23
A1	01	62	49	52	42	92	08	89	55	24	5	67	36	51	14	11	54	86
LAD	37.	45.	126	164	238	707	133	532	612	51.	242		223	587	858	260	410	127
HMF	276	893	.74	2.3	0.6	9.8	96.	68.	72.	149	.09	342	9.2	1.5	7.1	58.	72.	934
A1	75	58	61	92	07	48	62	61	6	8	35	.07	72	08	96	87	28	.1

Table 3: AMSE of the estimators when $n = 20$ and $\sigma_{outlier}^2$ (magnitude of outliers) = 250

	NUMBER OF EXPLANATORY VARIABLES	
	3	5



Global Journal of Engineering Science and Research Management

ESTI MAT ORS	DEGREES OF MULTICOLLINEARITY									DEGREES OF MULTICOLLINEARITY								
	0.900			0.990			0.999			0.900			0.990			0.999		
	% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS		
	5%	10%	20%	5%	10%	20%	5%	10%	20%	5%	10%	20%	5%	10%	20%	5%	10%	20%
OLS	177	267	431	961	276	328	653	237	308	139	261	355	214	235	420	132	302	106
	1.5	9.8	2.2	3.3	35.	99.	19.	416	577	7.7	5.2	6.3	00.	09.	12.	132	069	440
	25	18	93	39	54	69	7	.3	.8	75	3	34	49	84	5	156	.6	8
MMI NFA2	162	246	397	882	253	303	604	218		129	242	329	198	217	389		279	987
	4.5	4.2	1.2	4.3	50.	87.	88.	721	283	1.3	4.9	0.3	85.	24.	62.	122	114	196
	37	88	27	47	21	7	01	.7	887	49	39	93	47	99	87	108	.9	.7
MMA XFA2	710	125	198	317	903	161	300	924		590	122	197	852	927	190	458	121	554
	.31	7.1	4.9	7.6	2.3	15.	32.	70.	126	.57	6.0	2.6	7.0	7.9	77.	51.	976	436
	04	69	48	55	38	32	26	17	838	11	01	93	64	26	98	28	.5	.4
MMI DFA2	777	139	216	324	919	165	300	927	127	629	134	210	858	939	193	459		554
	.39	8.5	0.8	6.7	2.4	30.	89.	40.	210	.90	2.0	8.8	3.0	8.1	17.	01.	122	680
	22	98	13	86	57	66	02	03	.8	82	22	98	84	35	1	92	061	.9
MMF A2	155	217	349	819	211	290	542	190	269	107	205	315	178	184	338	105	222	793
	8.4	4.2	1.3	8.2	85.	72.	43.	449	532	6.5	0.8	2.3	36.	66.	48.	456	139	526
	34	27	83	77	78	79	75	.4	.3	74	71	83	54	77	75	.9	.9	.4
MGM FA2	129	196	310	585	154	238	388	129	179	101	200	300	119	137	260	548	134	581
	0.2	5.1	5.9	7.9	30.	43.	79.	289	816	4.6	5.5	2.7	56.	04.	14.	36.	334	141
	47	67	17	47	67	79	5	.3	.6	35	49	73	35	05	84	35	.6	.9
MHM FA2	165	246	394	949	273	324	651	237	308	132	247	330	213	233	416	132		106
	9.2	1.1	3.1	2.8	89.	16.	97.	165	115	6.5	4.9	1.3	22.	42.	87.	074	301	406
	04	44	73	82	34	85	68	.5	.3	74	39	41	07	23	99	.4	908	4
MMI NFA1	961	155	253	505	147	204	410	137	177	855	164	234	133	143	270	784		729
	.56	0.8	4.9	2.7	40.	37.	71.	865	475	.79	0.6	2.3	44.	21.	52.	17.	187	152
	99	5	14	77	07	25	85	.2	.3	15	16	17	84	43	98	46	002	.9
MMA XFA1	649	109	179	311	889	157	299	922	126	551	109	182	847	917	188	458	121	554
	.07	6.3	8.0	6.8	1.0	38.	79.	18.	485	.88	4.1	1.7	7.0	1.3	62.	04.	898	206
	86	83	18	32	44	24	57	18	.8	54	34	71	33	88	37	34	.1	.7
MMI DFA1	652	110	180	312	889	157	299	922	126	554	110	183	848	917	188	458	121	554
	.39	5.6	9.1	0.4	9.4	61.	82.	34.	508	.41	3.1	2.2	0.5	8.7	77.	07.	903	223
	86	51	29	57	72	95	84	13	.9	92	93	72	16	21	5	68	.7	.7
MMF A1	860	126	206	417	107	187		108	157	644	126	215	105	108	217	581	138	590
	.50	5.8	8.0	0.9	27.	11.	343	763	910	.45	3.1	9.9	48.	84.	84.	09.	031	063
	44	25	34	31	89	41	26	.8	.2	68	38	13	02	81	21	69	.8	.9
MGM FA1	710	118	193	331	937	164	305	946	129	619	124	204	872	955	195	463	122	555
	.47	7.8	3.3	6.2	3.0	41.	58.	57.	756	.54	2.4	4.1	9.6	8.6	08.	43.	670	919
	01	61	29	31	05	48	95	54	.6	27	6	99	81	4	12	31	.5	.7
MHM FA1	103	151	243	807	242	276	634	233	301	914	171	232	203	214	381	130	299	105
	6.3	4.6	0.2	9.8	91.	72.	34.	328	153	.50	3.2	9.8	57.	33.	66.	955	695	933
	07	19	38	46	18	59	79	.4	.8	46	31	71	87	36	17	.8	.7	0
MM MINF A2	161	244	393	880	252	300	597	216	281	128	241	323	197	215	385	121	276	
	7.2	9.3	8.4	7.8	45.	04.	25.	951	497	4.5	0.9	9.2	42.	75.	67.	566	685	970
	09	48	8	34	17	49		.9	.5	77	01	13	79	35	7	.2	.9	562
MM MAX FA2	545	851	110	245	613	653		478	481	378	816	856	520	473	628	302	610	146
	.84	.54	4.1	2.1	7.4	4.7	166	41.	91.	.03	.10	.41	4.2	3.8	6.1	83.	06.	730
	44	26	49	18	83	13	70	72	06	76	42	36	61	48	44	15	49	.4
MM MID FA2	626	105	137	253	633	725	167	481	487	429	987	113	527	489	668	303	611	147
	.09	1.1	1.2	0.6	0.3	1.9	40.	55.	05.	.54	.32	1.5	2.8	3.9	4.1	39.	20.	126
	45	93	84	69	68	18	27	71	1	59	75	52	2	05	38	33	91	.2
MM MFA 2	154	210	333	814	205	282	512	181	263	102		304	172	175	315	102	203	633
	4.3	2.7	1.4	4.9	77.	46.	78.	945	929	6.1	195	2.9	48.	41.	44.	569	539	092
	2	5	58	86	51	59	55	11	.8	.7	73	8.7	54	5	77	05	.9	.1
MMG MFA 2	123	183	279	555	138	201	289	984	133	946	190	281	960	110	187	409	790	197
	6.5	3.5	4.4	2.7	37.	49.	50.	80.	161	.26	0.6	0.7	3.5	13.	47.	08.	89.	829
	5	01	87	68	02	85	3	81	.4	68	8	19	89	57	37	99	93	.1
MMH MFA 2	165	244	390	949	273	324	651	237	308	132	246	325	213	233	416	132	301	106
	5.0	5.9	8.2	2.5	87.	01.	97.	165	114	3.7	6.3	9.4	21.	40.	83.	074	907	406
	1	5	21	31	7	65	19	.2	.3	1	4	07	72	82	18	.4	.8	3
MM MINF A1	846	126	194	463	130	142	321	110	129	734	141	160	114	118	205	698	155	502
	.56	6.2	4.7	0.9	15.	43.	39.	510	396	.53	2.7	3.5	23.	86.	49.	06.	079	384
	98	22	33	13	62	83	89	.3	.4	07	81	64	21	29	73	33	.1	.2



Global Journal of Engineering Science and Research Management

MM	473	631	834	238	596	591	166	475	477	328	623	574	514	459	595	302	609	146
MAX	.00	.37	.51	4.2	9.0	8.9	05.	54.	18.	.87	.19	.89	3.5	6.0	5.8	31.	01.	366
FA1	11	67	01	16	06	35	23	97	25	65	31	26	02	16	92	21	04	.5
MM	476	643	849	238	597	595	166	475	477	332	635	591	514	460	597	302	609	146
MID	.92	.47	.15	8.2	8.9	4.2	09.	72.	47.	.02	.77	.83	7.7	5.3	7.4	34.	08.	392
FA1	04	03	49	15	82	27	24	72	8	47	76	1	15	32	03	9	53	.3
MM	725	863	122	360	819	111	224	696	975	448	871	123	777	698	111	448	845	215
MFA	.62	.69	9.7	7.5	5.7	51.	52.	69.	76.	.83	.16	5.3	1.5	3.8	54.	80.	67.	772
I	63	48	26	66	73	42	85	05	06	97	39	83	46	61	39	72	8	.9
MMG	546	754	102	261	654	709	173	505	523		840	100	545	511	701	308	619	149
MFA	.03	.92	7.1	0.4	9.0	6.2	36.	07.	75.	415	.52	0.1	4.0	2.1	4.4	34.	60.	194
I	52	35	1	32	68	98	26	04	08	.87	48	48	01	55	88	16	28	.7
MMH	939	121	179	800	240	262	633	233	300	822	149	160	203	212	376	130	299	105
MFA	.02	8.0	9.9	9.9	84.	94.	28.	241	911	.40	6.3	0.4	07.	61.	05.	947	667	926
I	82	75	34	33	93	7	8	.9	.3	84	92	25	53	74	18	.9	.9	7
SMIN	162		394	885	253	300	601	218	282		242	324	198	216	386	122	278	972
FA2	6.1	245	5.4	4.0	52.	72.	98.	019	079	129	3.1	6.4	59.	57.	33.	349	024	503
	65	9.1	62	28	02	3	05	.1	.1	0.9	66	74	88	65	81	.8	.7	.9
SMA	748	108	133	360	905	858	271	754	692	551	109	109	834	739	940	505	104	210
XFA2	.97	1.6	6.9	7.8	5.0	8.9	43.	67.	18.	.17	2.6	5.1	5.2	7.1	1.5	45.	436	394
	63	98	05	57	28	66	68	33	1	32	19	47	43	08	47	05	.2	.7
SMID	813	124	157	367	921	924	271	757	697	591	123	133		753	977	505	104	210
FA2	.07	6.6	7.6	4.4	6.6	4.5	95.	45.	23.	.50	5.6	9.3	840	3.4	9.7	93.	534	775
	23	37	2	38	66	27	67	82	05	94	55	58	1.8	82	69	32	.5	.5
SMF	156	214	336	826	211	284	532	187		106	203	305	177	180	320	106	216	655
A2	1.4	5.2	8.8	5.4	92.	01.	63.	090	265	8.1	3.5	9.9	39.	75.	38.	556	184	901
	68	94	39	36	01	05	52	.9	338	57	2	74	69	75	14	.5	.7	.2
SGM	130	190	287	609	154	209	362	117	146	100	198	284	117	126	205	589		257
FA2	1.7	9.2	0.5	3.8	56.	20.	68.	229	108	2.2	5.2	3.0	68.	02.	52.	56.	118	515
	38	35	34	73	61	36	89	.3	.6	25	23	1	28	88	87	65	839	.5
SHM	166	245	391	949	273	324	651	237	308	132	247	326	213	233	416	132	301	106
FA2	0.3	6.4	5.7	3.9	89.	03.	97.	165	114	6.4	1.7	5.3	22.	41.	83.	074	907	406
	78	93	73	33	16	93	52	.4	.5	9	1	15	06	54	78	.5	.9	3
SMIN	988	142	209	535	147	155	386	127	142	831	158	175	131	133		810	177	
FA1	.02	5.9	5.3	1.5	68.	67.	52.	133	748	.35	5.0	5.6	59.	23.	221	67.	798	535
	8	08	92	34	65	41	64	.8	.1	83	22	3	46	48	50	64	.9	799
SMA	689	898	109	354	891	801	270	752	687	514	939	853	829	727	907	505	104	210
XFA1	.65	.65	1.5	8.4	2.0	8.6	95.	09.	48.	.95	.40	.72	4.6	8.9	5.7	00.	345	043
	91	03	17	15	79	83	71	92	63	51	33	24	14	56	84	26	.4	.1
SMID	692	909	110	355	892	805	270	752	687	514	939	853	829	728	909	505	104	210
FA1	.92	.05	5.1	1.9	0.6	1.9	98.	26.	78.	.53	.28	.04	8.1	6.9	7.6	03.	351	068
	26	92	46	9	29	56	68	07	48	41	81	84	43	72	14	45	.8	.2
SMF	892	109	145	453	107	127	314	936	114	606	113	143	103	928	138	620	123	273
A1	.08	1.7	0.0	7.9	60.	75.	28.	06.	342	.57	8.8	0.9	63.	0.8	23.	10.	097	907
	23	09	95	44	94	17	64	75	.4	7	35	57	84	81	06	6	.9	.1
SGM	749	100	126	374	939	910	276	777	732	580	111	122	854	771	100	510	105	212
FA1	.12	2.0	7.3	0.6	8.7	2.6	36.	77.	54.	.82	3.1	3.1	9.3	8.4	87.	12.	244	748
	96	73	44	7	3	65	13	36	14	2	45	17	5	42	88	72	.7	.8
SHM	105	139	196	814	242	265	633	233	300	901	163	174	203	213	376	130	299	105
FA1	9.8	3.2	3.7	3.9	81.	50.	98.	294	962	.11	5.3	8.5	55.	56.	97.	959	680	927
	68	82	09	9	95	91	9	.4	.3	13	15	25	34	24	14	.3	.7	3
LTSM	163	248		895	256	303	608	220	284	130	245	328	201	219	390	124	282	985
INFA	8.9	1.1	398	5.2	22.	95.	38.	067	219	7.8	7.2	7.2	69.	48.	50.	688	462	863
2	24	94	4.2	26	65	38	03	.3	.5	65	74	75	14	55	72	.7	.2	.4
LTSM	939	143	212	526	133	151	382		121	803	159	183	132	127	194	829	172	498
AXFA	.30	6.9	7.1	7.7	45.	97.	50.	110	330	.89	3.2	3.5	38.	69.	29.	90.	343	649
2	47	75	2	54	97	09	72	725	.6	17	87	01	71	99	63	27	.8	.9
LTSM	987	155	229	531	134	156	382	110	121	828	167	198	132	128	196		172	498
IDFA	.79	5.6	0.6	2.8	74.	45.	89.	958	720	.86	9.1	7.3	72.	54.	70.	830	405	914
2	17	62	68	64	85	66	9	.4	.8	64	99	39	96	74	97	18	.8	.5
LTSM	158	222	353	849	223	290	556	194	269	114	218	314	187	193	341	114	241	771
FA2	3.4	6.4	5.1	5.6	47.	61.	41.	895	984	5.0	6.2	3.0	59.	96.	38.	793	100	092
	64	93	75	48	2	72	7	.9	.7	51	24	46	2	81	98	.7	.2	.2



Global Journal of Engineering Science and Research Management

LTSG	136	204	317	694	180	235	444	142	177	109	215	298	152	158	264	876	181	528
MFA	9.4	4.3	5.6	4.6	89.	87.	15.	124	627	9.1	4.2	3.6	29.	77.	60.	91.	150	326
2	44	77	65	27	24	98	88	.7	.8	87	38	15	69	88	61	87	.5	.2
LTSH	166	247	395	949	273	324	651	237	308	133	249	330	213	233	416	132	301	106
MFA	9.5	9.5	7.3	9.7	95.	20.	98.	166	115	5.9	2.1	0.9	24.	46.	90.	074	908	406
2	92	41	52	25	85	52	34	.4	.7	81	33	16	35	57	14	.9	.4	4
LTSM	112	168	264	643	175	199	459	149	175	983	189	225	160	163	274	100		696
INFA	1.8	5.5	1.0	9.7	86.	07.	47.	432	152	.48	5.9	1.9	31.	23.	92.	068	217	868
1	36	91	75	21	94	46	12	.4	.7	37	78	26	58	97	74	.9	154	.2
LTSM	894	130	195	522	132	147	382	110	120	779	149	166	132	126	192	829	172	498
AXFA	.41	3.9	6.2	7.2	28.	99.	14.	507	966	.82	5.2	7.7	07.	93.	17.	64.	286	404
1	85	83	14	73	91	2	41	.4	.5	9	34	42	78	66	42	51	.3	.5
LTSM	896	131	196	522	132	148	382	110	120	781	150	167	132	126	192	829	172	498
IDFA	.90	1.8	6.0	9.7	36.	22.	16.	521	989	.41	1.9	8.6	09.	98.	31.	66.	290	422
1	66	5	73	16	03	84	66	.1	.7	14	75	63	94	97	84	34	.4	.1
LTSM	104	144	220	589	146	180	412	124	154	838	162	204	144	138	221	893		538
FA1	7.9	4.1	4.2	2.4	47.	23.	48.	665	385	.27	0.8	5.1	19.	83.	97.	91.	183	313
	85	69	13	54	68	81	16	.4	.1	2	55	82	74	4	29	14	734	.3
LTSG	939	137	207	535	136	155	386		124	822	160	191	133	129	198	832	172	500
MFA	.42	9.6	9.4	7.5	17.	49.	16.	112	402	.22	5.5	4.1	61.	66.	65.	57.	851	263
1	04	99	44	81	34	06	2	612	.3	08	11	05	36	69	56	67	.5	.2
LTSH	118	166	254	839	247	276	635	233	301	103	192	224	205	217	382	131	299	105
MFA	2.4	4.3	3.1	4.6	35.	20.	21.	466	211	4.6	7.2	5.7	20.	03.	68.	034	769	934
1	84	9	37	47	5	54	65	.3	.6	44	48	4	85	35	3	.1	.6	6
LMS	165	250	400	904	258	306	616	222	286	134	251	336	206	224	397	127	288	100
MINF	5.6	2.2	9.5	8.5	71.	43.	63.	611	399	4.9	6.6	5.0	64.	51.	66.	712	575	780
A2	37	35	26	72	61	84	81	.9	.7	4	88	37	57	12	18	.9	.6	4
LMS	111	165	245	634	164	181	445	144	155	113	212	258	174	176	289	108	229	727
MAX	9.0	9.0	0.2	9.4	73.	77.	28.	922	118	2.9	7.7	0.1	84.	01.	62.	560	229	178
FA2	6	96	43	92	34	56	11	.8	.6	4	99	71	41	11	18	.5	051	.3
LMS	115	175	258	638	165	185	445		155	114	216	265		176	290	108	229	727
MID	5.5	2.8	5.6	2.4	67.	28.	59.	145	433	3.5	4.0	8.4	174	41.	89.	573	085	727
FA2	13	89	65	48	9	02	52	076	.2	71	14	66	99	9	44	.6	.1	334
LMS	161	229	362	869	232	295	577	203	274	127	238	327	199	210	367	122	264	880
MFA	0.6	0.5	0.4	0.8	80.	01.	35.	460	190	3.8	6.5	7.6	68.	13.	56.	890	809	275
2	04	81	32	63	15	23	7	.4	.8	95	99	2	36	67	46	.1	.6	.3
LMS	144	214	331	755	200	249	492	166		125	237	318	183	191	325	110	233	744
GMF	3.3	3.0	7.3	1.6	49.	29.	20.	018	199	5.1	2.0	5.5	34.	58.	97.	676	616	744
A2	53	96	6	07	78	02	95	.7	413	32	57	84	14	05	73	.5	.2	576
LMS	168	250	398	950	274	324	652	237	308	135	253	337	213	233	417	132	301	106
HMF	1.1	1.1	5.2	5.7	04.	40.	00.	169	118	8.2	3.8	1.7	35.	68.	17.	078	913	406
A2	09	03	3	19	44	64	88	.5	.4	55	76	51	72	33	3	.5	.4	7
LMS	125	185	287	719	196	219	503	171	197	120	225	279	186	193	331	116	252	838
MINF	5.8	6.1	4.2	0.8	71.	24.	87.	073	461	8.0	7.3	3.9	92.	88.	37.	161	071	875
A1	23	48	86	93	3	78	18	.5	.9	81	16	55	57	21	98	.3	.7	.5
LMS	108	155	230	631	163	178	444	144		112	208	249	174	175	288	108	229	727
MAX	4.5	6.2	7.6	9.8	89.	67.	98.	779	154	2.6	7.4	5.3	71.	64.	48.	548	019	727
FA1	15	59	58	62	2	28	75	.3	824	23	09	51	14	56	42	.4	.3	034
LMS	108	156	231	632	163	178	445	144	154	112	209	250	174	175	288	108	229	727
MID	6.4	2.1	5.8	1.6	94.	85.	00.	788	842	3.3	0.1	1.0	72.	67.	56.	549	021	044
FA1	84	21	85	52	25	86	6	.5	.8	11	04	32	07	1	25	.3	.6	.3
LMS	120	166	251	680	174	204	468	154	181	114	213	268	179	181	303	111	234	750
MFA	0.5	4.7	4.1	0.4	51.	10.	15.	144	138	7.5	9.3	7.9	82.	47.	93.	427	931	340
1	32	55	93	64	48	4	71	.7	.6	68	68	63	35	29	52	.5	.5	.3
LMS	111	161	241	641	166	184	448	146	157	114	213	262	175	176	291	108	229	728
GMF	9.1	4.2	0.5	5.0	73.	52.	16.	160	578	0.7	2.9	1.1	36.	96.	91.	685	327	128
A1	48	47	65	44	78	42	12	.4	.3	44	22	78	32	07	16	.8	.3	.8
LMS	130	183	279	860	251	283	637	233	301	122	227	278	208	223	392	131	300	105
HMF	1.6	8.3	3.0	5.4	18.	01.	32.	752	545	3.8	0.6	9.0	37.	02.	60.	272	128	970
A1	21	74	36	75	66	1	68	.5	.7	98	1	39	93	85	38	.9	.9	7
LAD	160	243	392	875	251	298	593		280	127	239	323	196	214	384	120	275	967
MINF	6.6	6.7	2.5	0.5	19.	84.	12.	215	491	7.2	8.8	0.7	10.	77.	45.	893	218	345
A2	18	36	01	2	66	71	34	805	.3	7	13	86	47	92	78	.2	.7	.4



Global Journal of Engineering Science and Research Management

LAD	78.	285	305	39.	83.	373	71.	92.	124	53.	243	377	39.	56.	151	70.	57.	659
MAX	899	.46	.13	477	306	.91	708	923	.51	255	.47	.27	359	737	.96	768	680	2.8
FA2	39	78	75	18	82	53	25	27	89	29	96	35	72	62	1	58	01	81
LAD	192	574	656	95.	213	101	88.	162	222	122	489	711	70.	158	432	78.	72.	664
MID	.19	.20	.19	055	.72	7.7	006	.44	.61	.17	.21	.15	170	.54	.36	380	159	2.4
FA2	63	39	28	45	68	64	44	37	3	79	91	42	63	25	49	58	6	03
LAD	152	202	323	797	195	279	489	174	261	962	185	302	165	167	305	980	185	576
MFA	2.0	9.9	0.5	2.7	71.	44.	17.	431	302	.34	1.4	0.5	83.	33.	55.	52.	667	529
2	34	22	72	18	45	14	5	.2	.6	68	08	17	34	61	21	43	.2	.2
LAD	112	168	256	446	104	180	163	617	100	856	177	276	588	808	148	117	179	501
GMF	3.0	4.2	6.8	8.3	09.	89.	71.	21.	824	.39	5.6	3.2	1.2	4.6	41.	60.	80.	49.
A2	9	22	54	29	53	85	28	71	.6	28	81	59	39	94	77	1	25	56
LAD	164	243	388	949	273	323				132	245	325	213	233	416	132	301	106
HMF	8.2	1.1	7.1	0.9	86.	98.	651	237	308	0.4	9.8	0.9	21.	40.	82.	074	907	406
A2	55	17	09	56	26	06	97	165	114	62	78	43	43	09	18	.4	.8	3
LAD	538	889	144	308	923	101	212	785	958	561	110	130	855	928	171	533	120	414
MINF	.05	.34	0.1	7.9	3.3	62.	55.	06.	84.	.58	4.1	7.0	1.5	1.3	10.	61.	044	371
A1	09	91	88	79	16	42	97	95	98	99	45	19	69	54	39	31	.1	.9
LAD	4.9	11.	13.	7.2	10.	31.	56.	28.	28.	2.7	8.3	95.	21.	6.5	11.	62.	43.	654
MAX	763	662	650	962	552	765	605	854	028	271	428	731	317	344	441	288	317	3.9
FA1	8	27	62	03	74	54	52	13	88	09	76	19	16	62	99	42	14	59
LAD	8.3	23.	27.	10.	16.	52.	58.	40.	46.	4.8	18.	107	23.	9.8	19.	63.	45.	655
MID	784	952	297	314	881	717	883	385	933	223	928	.94	081	018	719	718	800	2.6
FA1	57	28	72	17	42	83	54	13	09	13	14	71	73	66	47	13	48	42
LAD	346	302	467	152	240	591	666	227	541	149	321	841	319	259	536	173	248	694
MFA	.48	.62	.10	9.2	6.2	9.0	7.9	60.	26.	.22	.52	.31	6.2	5.6	4.7	47.	13.	35.
1	6	36	21	6	42	69	86	51	76	91	84	44	55	78	44	89	58	61
LAD	79.	153	210	168	407	862	405	139	197	103	277	548	198	345	717	227	321	717
GMF	143	.63	.84	.87	.67	.33	.86	7.3	1.4	.29	.90	.89	.55	.13	.12	.30	.82	4.8
A1	23	28	01	82	15	05	49	37	02	59	79	62	91	58	17	71	85	29
LAD	673		118		238	257	632	233	300	682	121	129	202	211	374	130		105
HMF	.71	786	9.5	781	17.	17.	80.	198	832	.10	7.5	1.2	59.	44.	39.	939	299	925
A1	63	.41	54	3.9	33	22	31	.2	.5	02	85	5	43	93	66	.4	656	8

Table 4: AMSE of the estimators when $n = 40$ and $\sigma_{outlier}^2$ (magnitude of outliers) = 10

ESTI MAT ORS	NUMBER OF EXPLANATORY VARIABLES																	
	3									5								
	DEGREES OF MULTICOLLINEARITY									DEGREES OF MULTICOLLINEARITY								
	0.900			0.990			0.999			0.900			0.990			0.999		
	% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS		
5%	10	20	5%	10	20	5%	10	20	5%	10	20	5%	10	20	5%	10	20	
OLS	0.7	1.7	2.7	11.	15.	37.	117	136	365	1.0	2.0	4.3	14.	24.	38.	124	274	579
	755	504	916	184	992	935	.14	.82	.03	648	578	706	157	080	973	.50	.21	.69
	81	74	44	9	25	88	4	88	73	12	15	66	94	38	84	23	08	25
MMI NFA2	0.7	1.6	2.6	10.	15.	36.	112	131	349	1.0	1.9	4.2	13.	23.	37.	119	263	557
	433	790	812	732	333	427	.33	.27	.96	272	827	219	621	161	615	.92	.93	.89
	07	61	4	44	4	73	46	97	46	76	32	55	44	64	19	9	42	6
MMA XFA2	0.4	0.9	1.6	4.0	6.4	16.	40.	50.	153	0.5	1.1	2.3	5.5	9.7	17.	47.	108	255
	458	288	525	810	590	767	425	838	.64	262	062	636	325	100	731	756	.85	.14
	65	06	34	49	83	17	66	16	42	07	59	25	25	92	03	29	75	71
MMI DFA2	0.5	1.0	1.8	4.2	6.7	17.	40.	51.	154	0.5	1.2	2.6	5.7	9.8	18.	47.	109	255
	137	863	848	446	957	252	578	251	.24	982	216	230	475	613	123	859	.17	.64
	49	92	41	77	59	21	55	38	21	38	54	51	66	2	94	03	33	25
MMF A2	0.7	1.5	2.5	9.8	14.	34.	106	123	315	0.9	1.7	3.9	11.	20.	34.	106	229	485
	293	685	897	506	411	606	.92	.85	.94	296	280	352	939	029	924	.42	.65	.68
	5	37	66	06	61	04	7	47	28	51	79	69	24	46	19	59	96	82
MGM FA2	0.6	1.4	2.4	7.9	12.	28.	71.	89.	229	0.9	1.7	3.9	9.7	16.	29.	65.	144	319
	756	697	227	441	026	567	069	829	.37	474	955	494	357	092	419	782	.13	.08
	81	58	46	96	13	28	69	88	33	84	22	29	75	96	67	76	75	23
MHM FA2	0.6	1.6	2.5	11.	15.	37.	117	136	364	1.0	1.9	4.1	14.	23.	38.	124	274	579
	992	028	158	073	802	577	.03	.63	.65	061	487	519	089	958	741	.43	.08	.44
	06	94	8	65	69	08	98	58	34	24	61	87	49	87	07	42	36	77



Global Journal of Engineering Science and Research Management

MMI	0.4	0.9	1.6	6.1	9.0	22.	63.	76.	216	0.6	1.3	2.8	8.6	14.	25.	77.	167	373
NFAI	476	829	780	687	039	617	341	751	.45	580	439	503	789	967	170	113	.91	.77
MMA	0.3	0.6	1.2	3.9	6.1	16.	40.	50.	153	0.4	0.9	2.0	5.3	9.5	17.	47.	108	254
XFAI	340	713	574	291	419	312	279	449	.07	214	229	096	294	710	365	658	.55	.67
MMI	0.3	0.6	1.2	3.9	6.1	16.	40.	50.	153	0.4	0.9	2.0	5.3	9.5	17.	47.	108	254
DFAI	371	792	691	330	501	16.	283	460	.08	247	291	201	350	749	375	660	.56	.68
MMF	0.4	0.7	1.4	4.7	7.3	19.	51.	62.	172	0.4	1.0	2.3	6.3	11.	20.	56.	123	286
A1	143	941	896	185	619	257	578	319	.80	957	283	239	115	013	381	492	.46	.75
MGM	0.3	0.7	1.3	4.1	6.4	16.	41.	52.	156	0.5	1.0	2.3	5.6	9.9	18.	48.	109	256
FAI	648	392	623	354	639	959	316	015	.04	095	667	366	254	733	174	258	.72	.90
MHM	0.3	0.8	1.4	8.6	11.	30.	113	130	0.5	1.1	2.5	12.	20.	33.	122	269	571	
FAI	782	21	3	36	16	27	54	47	.01	65	37	43	52	35	66	07	.48	.93
MM	0.7	1.6	2.6	10.	15.	36.	112	131	349	1.0	1.9	4.2	13.	23.	37.	119	263	556
MINF	427	773	764	722	311	351	.23	.14	.22	264	788	135	610	125	553	.79	.55	.67
A2	32	79	75	77	41	92	08	29	46	2	45	29	89	16	78	49	03	17
MM	0.4	0.7	1.3	2.8	3.9	8.9	29.	32.	79.	0.4	0.8	1.5	4.2	5.8	8.8	33.	67.	120
MAX	045	947	383	784	093	596	296	266	401	361	212	664	967	670	723	660	207	.67
FA2	82	49	4	44	67	02	25	34	49	13	61	61	27	77	12	04	5	32
MM	0.4	0.9	1.6	3.0	4.3	9.6	29.	32.	80.	0.5	0.9	1.9	4.5	6.0	9.4	33.	67.	121
MID	853	893	659	731	609	767	475	762	187	247	799	746	598	648	739	781	595	.33
FA2	45	73	82	97	53	88	11	29	64	9	39	65	06	52	38	92	84	42
MM	0.7	1.5	2.5	9.7	14.	34.	106	123	309	0.9	1.6	3.8	11.	19.	34.	104	224	466
MFA	281	585	747	778	296	271	.51	.15	.28	204	711	729	799	479	424	.84	.20	.83
2	95	76	27	59	04	84	03	92	78	36	31	59	18	26	49	52	65	54
MMG	0.6	1.4	2.3	7.5	11.	26.	65.	82.	190	0.9	1.7	3.8	9.2	14.	27.	56.	113	218
MFA	706	476	768	935	414	460	801	570	.25	403	571	907	996	413	024	154	.82	.62
2	6	75	51	74	67	01	87	71	77	38	36	33	17	54	9	82	82	65
MMH	0.6	1.5	2.4	11.	15.	37.	117	136	364	1.0	1.9	4.1	14.	23.	38.	124	274	579
MFA	961	962	887	073	800	572	.03	.63	.65	043	428	377	089	958	739	.43	.08	.44
2	37	51	88	03	88	93	97	56	3	97	68	76	33	34	45	41	35	76
MM	0.4	0.8	1.3	5.4	7.4	17.	56.	65.	171	0.5	1.1	2.3	8.0	12.	20.	70.	145	302
MINF	066	615	745	436	074	840	675	778	.15	983	495	275	705	918	675	016	.37	.70
A1	66	53	95	13	97	25	77	23	4	29	66	87	98	07	9	15	17	25
MM	0.2	0.4	0.7	2.7	3.5	8.3	29.	31.	78.	0.3	0.5	1.0	4.0	5.6	8.3	33.	66.	120
MAX	756	919	884	040	101	173	125	807	660	119	784	267	539	912	447	544	842	.05
FA1	24	66	39	81	86	09	48	93	89	71	54	03	6	23	79	31	96	23
MM	0.2	0.5	0.8	2.7	3.5	8.3	29.	31.	78.	0.3	0.5	1.0	4.0	5.6	8.3	33.	66.	120
MID	788	001	029	084	197	336	130	820	681	154	857	409	603	960	587	547	853	.07
FA1	4	18	03	72	7	58	18	28	09	56	95	94	84	12	62	67	48	02
MM	0.3	0.6	1.1	3.6	5.1	12.	42.	46.	106	0.3	0.7	1.5	5.2	7.6	13.	44.	86.	168
MFA	670	308	064	513	392	731	644	931	.41	988	153	038	503	165	094	587	312	.61
1	86	68	12	85	56	59	67	11	43	57	96	61	34	04	64	4	89	72
MMG	0.3	0.5	0.9	2.9	3.9	9.2	30.	33.	82.	0.4	0.7	1.5	4.4	6.2	9.5	34.	68.	123
MFA	090	665	274	426	158	408	344	695	601	156	673	238	101	135	525	262	276	.05
1	58	17	68	61	23	04	64	44	88	87	71	96	44	57	11	29	67	99
MMH	0.3	0.6	0.9	8.3	11.	28.	113	130	351	0.4	0.9	1.8	12.	20.	32.	122	269	571
MFA	249	566	905	919	388	566	.46	.16	.51	784	173	549	232	615	463	.18	.85	.28
1	57	13	48	7	21	89	36	11	29	94	02	23	85	07	6	45	65	46
SMIN	0.7	1.6	2.6	10.	15.	36.	112	131	349	1.0	1.9	4.2	13.	23.	37.	120	263	557
FA2	439	793	783	743	336	378	.48	.28	.41	278	826	163	634	168	578	.120	.90	.11
FA2	33	12	35	67	11	29	15	96	22	91	39	41	84	04	84	.02	24	99
SMA	0.4	0.9	1.4	4.5	6.2	11.	49.	48.	105	0.5	1.0	1.8	6.2	9.7	11.	50.	103	174
XFA2	577	088	333	903	187	661	834	364	.39	514	419	541	309	334	938	488	.18	.80
FA2	46	96	97	34	86	13	59	65	8	52	29	06	26	41	85	86	79	84
SMID	0.5	1.0	1.7	4.7	6.5	12.	49.	48.	106	0.6	1.1	2.2	6.4	9.8	12.	50.	103	175
FA2	230	732	354	447	789	280	964	781	.09	190	669	052	204	874	463	588	.50	.39
FA2	82	48	97	49	97	61	28	52	82	19	18	48	95	42	56	45	71	89



Global Journal of Engineering Science and Research Management

SMF A2	0.7 304 59	1.5 689 1	2.5 804 31	9.9 146 71	14. 419 65	34. 386 64	107 .45 94	123 .86 95	311 .26 26	0.9 339 95	1.7 191 21	3.8 940 62	12. 056 47	20. 069 57	34. 611 64	107 .13 38	228 .92 26	474 .04 49
SGM FA2	0.6 789 98	1.4 692 11	2.3 934 48	8.1 678 17	12. 028 32	27. 171 43	76. 146 07	89. 068 41	203 .88 1	0.9 510 54	1.7 903 18	3.9 106 106	10. 022 48	16. 153 18	27. 858 1	68. 125 34	139 .61 05	259 .16 4
SHM FA2	0.7 013 67	1.6 031 42	2.4 972 44	11. 074 31	15. 802 88	37. 574 37	117 .03 99	136 .63 58	364 .65 31	1.0 073 96	1.9 485 02	4.1 426 51	14. 089 74	23. 959 01	38. 740 09	124 .43 42	274 .08 36	579 .44 76
SMIN FA1	0.4 594 14	0.9 651 95	1.4 668 66	6.5 466 93	8.9 260 22	19. 448 18	69. 536 04	75. 366 34	187 .07 44	0.6 754 81	1.3 010 38	2.5 116 28	9.0 545 96	15. 029 71	22. 213 17	79. 090 39	164 .42 88	331 .18 62
SMA XFA1	0.3 586 59	0.6 559 95	0.9 264 06	4.4 509 08	5.8 899 88	11. 110 7	49. 710 7	47. 974 37	104 .74 25	0.4 574 63	0.8 514 84	1.3 914 63	6.0 563 87	9.5 923 93	11. 471 79	50. 393 79	102 .88 58	174 .25 07
SMID FA1	0.3 608 49	0.6 624 1	0.9 393 84	4.4 544 27	5.8 981 27	11. 124 01	49. 714 11	47. 985 01	104 .76 03	0.4 600 83	0.8 573 43	1.4 039 84	6.0 609 93	9.5 963 25	11. 484 35	50. 396 56	102 .89 45	174 .26 69
SMF A1	0.4 279 36	0.7 709 86	1.2 82 82	5.1 950 13	7.1 874 14	14. 943 47	59. 445 53	60. 215 6	129 .79 36	0.5 231 76	0.9 589 5	1.8 005 29	6.9 215 01	11. 059 07	15. 595 5	59. 053 48	118 .19 81	216 .24 11
SGM FA1	0.3 829 28	0.7 170 11	1.0 534 72	4.6 414 16	6.2 239 97	11. 903 63	50. 593 91	49. 556 14	108 .26 62	0.5 359 43	0.9 996 44	1.8 176 7	6.3 126 01	10. 001 62	12. 531 8	50. 976 92	104 .06 17	176 .92 98
SHM FA1	0.3 952 49	0.7 936 65	1.1 088 07	8.7 534 22	11. 959 37	29. 083 16	113 .59 55	130 .35 37	351 .64 17	0.5 843 44	1.1 125 1	2.1 034 55	12. 413 96	20. 942 59	32. 774 04	122 .23 19	269 .91 68	571 .33 7
LTSM INFA 2	0.7 458 6	1.6 834 59	2.6 849 27	10. 766 24	15. 372 51	36. 468 56	112 .74 78	131 .59 85	350 .27 06	1.0 306 67	1.9 870 33	4.2 249 17	13. 668 14	23. 229 58	37. 653 36	120 .36 67	264 .62 5	558 .46 37
LTSM AXFA 2	0.5 195 53	1.0 816 57	1.7 126 84	5.6 686 07	8.1 478 73	18. 309 76	61. 188 9	66. 337 25	173 .50 34	0.6 699 86	1.2 055 45	2.4 274 98	7.8 681 98	12. 875 61	18. 209 05	65. 972 38	137 .05 58	266 .04 75
LTSM IDFA 2	0.5 688 33	1.2 033 17	1.9 353 58	5.7 920 91	8.4 194 2	18. 755 39	61. 291 63	66. 658 94	173 .99 54	0.7 193 46	1.3 047 29	2.6 767 33	12. 8.0 054	18. 992 62	66. 581 09	137 049 83	266 .29 38	.49 .49 06
LTSM FA2	0.7 339 47	1.5 880 93	2.5 989 27	10. 035 21	14. 570 4	34. 746 38	108 .26 04	125 .10 57	318 .39 08	0.9 540 62	1.7 588 05	3.9 482 93	12. 342 23	20. 675 82	35. 087 51	109 .59 29	235 .42 22	488 .97 35
LTSG MFA 2	0.6 906 28	1.5 066 05	2.4 430 09	8.5 746 35	12. 612 54	29. 184 36	82. 088 12	97. 268 59	240 .36 93	0.9 674 24	1.8 190 69	3.9 619 49	10. 731 07	17. 700 65	29. 729 83	79. 299 32	164 .77 46	326 .34 3
LTSH MFA 2	0.7 090 48	1.6 159 69	2.5 267 09	11. 076 12	15. 806 58	37. 580 17	117 .04 01	136 .63 63	364 .65 37	1.0 123 71	1.9 559 03	4.1 576 86	14. 090 48	23. 960 3	38. 742 54	124 .43 43	274 .08 37	579 .44 78
LTSM INFA 1	0.5 208 05	1.1 232 53	1.7 371 95	7.2 480 75	10. 195 79	23. 739 34	76. 783 27	86. 811 98	228 .82 26	0.7 607 77	1.4 130 21	2.8 965 91	9.9 785 11	16. 864 92	25. 507 86	87. 649 43	184 .13 4	379 .36 7
LTSM AXFA 1	0.4 461 4	0.8 940 97	1.3 401 13	5.5 564 76	7.8 965 57	17. 903 74	61. 090 39	66. 035 85	173 .03 82	0.6 021 44	1.0 576 88	2.0 977 88	7.7 394 79	12. 768 99	17. 868 99	65. 898 26	136 .83 09	265 .62 58
LTSM IDFA 1	0.4 476 78	0.8 988 13	1.3 499 99	5.5 593 31	7.9 028 6	17. 914 06	61. 093 43	66. 043 58	173 .05 11	0.6 040 6	1.0 621 66	2.1 070 73	7.7 428 96	12. 771 76	17. 878 36	65. 900 42	136 .83 74	265 .63 81
LTSM FA1	0.4 972 3	0.9 796 73	1.5 560 39	6.1 530 86	8.8 770 33	20. 624 44	68. 772 33	75. 353 44	190 .03 24	0.6 494 5	1.1 407 17	2.3 896 23	8.3 688 96	13. 884 78	20. 769 98	72. 453 43	148 .36 51	295 .56 58
LTSG MFA 1	0.4 637 52	0.9 394 46	1.4 348 94	5.7 094 76	8.1 518 15	18. 485 82	61. 789 7	67. 254 88	175 .49 88	0.6 587 1	1.1 724 13	2.4 017 39	7.9 274 13	13. 079 51	18. 629 11	66. 350 36	137 .70 79	267 .62 61
LTSH MFA 1	0.4 728 54	0.9 934 59	1.4 734 18	9.0 500 62	12. 553 32	15. 513 83	113 .76 58	130 .71 21	352 .24 47	0.6 921 1	1.2 663 79	2.6 041 78	12. 619 67	21. 321 98	33. 568 32	122 .32 18	270 .05 54	571 .52 89



Global Journal of Engineering Science and Research Management

LMS	0.7	1.6	2.6	10.	15.	36.	112	131	350	1.0	1.9	4.2	13.	23.	37.	120	264	559
MINF	463	848	860	772	381	492	.83	.62	.46	317	893	276	694	264	673	.43	.88	.11
A2	39	32	85	87	08	76	32	83	42	32	54	04	03	6	88	15	31	34
LMS	0.5	1.1	1.7	6.1	8.5	19.	62.	67.	180	0.7	1.2	2.5	8.9	13.	19.	68.	152	290
MAX	352	233	584	269	343	389	808	808	.36	034	978	007	021	789	227	183	.17	.50
FA2	37	36	18	33	53	31	32	28	56	72	65	31	28	72	84	62	14	42
LMS	0.5	1.2	1.9	6.2	8.7	19.	62.	68.	180	0.7	1.3	2.7	9.0	13.	19.	68.	152	290
MID	800	360	683	356	978	812	908	108	.84	478	854	401	184	892	583	256	.38	.91
FA2	42	33	99	18	55	95	02	02	49	22	97	34	64	52	55	98	61	59
LMS	0.7	1.5	2.6	10.	14.	34.	108	125	319	0.9	1.7	3.9	12.	20.	35.	109	237	494
MFA	347	939	019	070	604	835	.49	.22	.33	602	811	616	539	908	197	.97	.79	.65
2	88	46	84	95	42	55	85	53	35	68	44	59	8	23	02	46	19	57
LMS	0.6	1.5	2.4	8.7	12.	29.	83.	97.	244	0.9	1.8	3.9	11.	18.	30.	80.	176	346
GMF	933	174	511	151	742	576	045	814	.08	725	350	747	228	146	116	735	.09	.10
A2	42	7	61	84	86	15	35	28	33	99	16	31	53	52	46	43	63	79
LMS	0.7	1.6	2.5	11.	15.	37.	117	136	364	1.0	1.9	4.1	14.	23.	38.	124	274	579
HMF	110	199	330	076	807	581	.04	.63	.65	142	595	618	091	961	743	.43	.08	.44
A2	69	38	79	65	39	94	02	64	39	61	17	57	07	28	4	43	38	79
LMS	0.5	1.1	1.7	7.5	10.	24.	77.	87.	233	0.7	1.4	2.9	10.	17.	26.	88.	192	394
MINF	363	618	814	217	478	476	859	520	.06	850	797	519	629	369	149	727	.71	.61
A1	67	81	97	93	13	69	13	15	92	06	57	02	72	66	51	22	11	41
LMS	0.4	0.9	1.4	6.0	8.2	18.	62.	67.	179	0.6	1.1	2.1	8.7	13.	18.	68.	151	290
MAX	706	493	105	276	848	997	712	527	.91	422	641	876	913	694	904	113	.96	.11
FA1	27	55	42	35	2	25	79	53	08	06	58	87	4	82	72	31	73	25
LMS	0.4	0.9		6.0	8.2	19.	62.	67.	179	0.6	1.1	2.1	8.7	13.	18.	68.	151	290
MID	718	537	1.4	301	912	007	715	535	.92	439	683	963	943	697	913	115	.97	.12
FA1	71	29	195	76	37	51	42	12	32	04	32	07	73	48	56	36	33	39
LMS	0.5	1.0	1.6	6.5	9.2	21.	70.	76.	196	0.6	1.2	2.4	9.3	14.	21.	74.	162	317
MFA	151	286	112	529	357	567	081	364	.18	849	397	644	233	671	674	263	.02	.83
1	7	87	31	18	27	73	79	17	03	68	35	63	38	38	56	06	11	4
LMS	0.4	0.9	1.4	6.1	8.5	19.	63.	68.	182	0.6	1.2	2.4	8.9	13.	19.	68.	152	291
GMF	855	914	979	629	382	556	388	664	.30	933	682	760	524	968	629	540	.75	.97
A1	52	2	29	41	1	57	8	53	09	17	39	6	65	49	52	82	74	16
LMS	0.4	1.0	1.5	9.1	12.	30.	113	130	352	0.7	1.3	2.6	12.	21.	33.	122	270	571
HMF	938	406	346	452	664	821	.82	.79	.40	227	441	711	746	497	725	.34	.11	.62
A1	53	44	94	33	63	13	11	51	44	59	89	46	77	24	19	59	46	64
LAD	0.7	1.6	2.6	10.	15.	36.	112	131	348	1.0	1.9	4.2	13.	23.	37.	119	263	556
MINF	421	761	743	717	303	326	.18	.04	.93	259	774	111	600	112	530	.74	.38	.24
A2	32	85	02	95	3	44	02	43	44	23	45	77	89	1	8	02	82	42
LAD	0.3	0.6	1.0	2.2	2.5	4.4	22.	17.	35.	0.3	0.6	1.1	2.9	3.8		24.	38.	56.
MAX	608	645	682	993	448	679	025	422	266	691	387	378	884	945	4.1	884	987	926
FA2	46	53	84	82	75	44	42	83	84	27	33	06	03	94	729	39	83	49
LAD	0.4	0.9	1.4	2.5	3.0	5.2	22.	17.	36.	0.4	0.8	1.6	3.2	4.1	4.8	25.	39.	57.
MID	557	008	951	190	696	851	208	946	078	715	296	416	783	176	652	012	408	628
FA2	34	52	57	52	2	49	47	94	76	03	61	8	56	58	99	5	91	4
LAD	0.7	1.5	2.5	9.7	14.	34.	106	122	306	0.9	1.6	3.8	11.	19.	34.	104	221	459
MFA	269	511	672	443	250	144	.30	.64	.19	145	432	517	642	245	212	.03	.27	.20
2	97	22	15	94	11	95	27	04	02	74	99	6	59	99	83	98	54	77
LAD	0.6	1.4	2.3	7.4	11.	25.	62.	76.	168	0.9	1.7	3.8	8.7	13.	25.	49.	93.	172
GMF	655	304	505	466	139	437	620	691	.27	358	394	709	645	628	841	885	659	.04
A2	18	03	71	91	64	1	54	37	34	49	64	22	87	58	71	95	29	56
LAD	0.6	1.5	2.4	11.	15.	37.	117	136	364	1.0	1.9	4.1	14.	23.	38.	124	274	579
HMF	926	903	714	072	800	571	.03	.63	.65	032	402	326	089	958	738	.43	.08	.44
A2	61	56	17	66	13	55	97	55	28	79	19	48	22	14	88	41	35	76
LAD	0.3	0.7	1.1	5.1	6.6	15.	52.	56.	145	0.5	1.0	2.0	7.3	11.	18.	65.	130	270
MINF	633	462	162	399	132	182	488	768	.29	558	330	710	212	943	318	484	.89	.62
A1	08	67	94	46	21	54	92	87	5	46	56	57	09	34	68	89	86	35
LAD	0.2	0.2	0.3	2.1	2.0	3.7	21.	16.	34.	0.2	0.3	0.4	2.7	3.7	3.5	24.	38.	56.
MAX	108	953	413	043	925	846	852	948	523	259	478	779	322	007	931	763	597	276
FA1	4	87	82	94	36	53	09	84	41	43	25	76	69	29	25	27	37	2
LAD	0.2	0.3	0.3	2.1	2.1	3.8	21.	16.	34.	0.2	0.3	0.4	2.7	3.7	3.6	24.	38.	56.
MID	142	043	585	092	030	009	856	961	543	298	561	938	387	059	078	766	608	294
FA1	97	01	09	43	42	45	83	46	45	63	78	44	06	06	12	78	56	85



Global Journal of Engineering Science and Research Management

LAD	0.3	0.4	0.7	3.1	3.9	8.9	36.	34.	66.	0.3	0.5	1.0	4.0	5.9	9.1	36.	61.	112
MFA	165	622	580	690	794	490	757	288	855	259	110	600	565	026	875	920	109	.91
I	38	55	71	11	1	34	66	98	26	78	07	4	94	04	74	27	8	77
LAD	0.2	0.3	0.5	2.3	2.5	4.7	23.	18.	38.	0.3	0.5	1.0	3.1	4.2	4.9	25.	40.	59.
GMF	484	830	184	717	523	839	115	956	684	454	737	849	125	870	569	521	157	499
AI	61	14	03	49	26	69	8	8	17	74	4	37	61	72	83	99	25	64
LAD	0.2	0.4		8.2	11.	27.	113	130	351	0.4	0.7	1.4	12.	20.	32.	122	269	571
HMF	667	885	0.5	720	097	873	.43	.03	.32	178	561	826	156	492	112	.17	.83	.23
AI	36	65	928	77	45	2	33	9	16	57	38	54	6	48	67	35	11	79

Table 5: AMSE of the estimators when $n = 40$ and $\sigma^2_{outlier}$ (magnitude of outliers) = 100

ESTI MAT ORS	NUMBER OF EXPLANATORY VARIABLES																	
	3									5								
	DEGREES OF MULTICOLLINEARITY									DEGREES OF MULTICOLLINEARITY								
	0.900			0.990			0.999			0.900			0.990			0.999		
	% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS		
	10	20		10	20		10	20		10	20		10	20		10	20	
	5%	%	%	5%	%	%	5%	%	%	5%	%	%	5%	%	%	5%	%	%
OLS	69.	112	295	676	320	249	578	164	354	129	169	325	991	178	336	135	224	479
	777	.53	.12	.01	3.2	5.6	9.7	84.	13.	.74	.47	.55	.30	5.6	5.4	13.	54.	46.
	81	74	51	55	49	43	47	54	41	87	41	3	06	19	75	33	33	82
MMI	66.	107	283	647	306	239	554	158	339	124	163	314	953	172	324	129	216	461
NFA2	923	.46	.35	.79	5.4	3.2	5.0	00.	60.	.87	.49	.15	.07	2.6	7.3	99.	38.	59.
	3	39	56	55	31	37	5	27	12	11	29	39	74	71	51	34	64	47
MMA	39.	76.	182	215	100	104	150	510	140	47.	90.	161	321	624	146	375	704	192
XFA2	617	180	.06	.15	3.2	7.4	4.4	7.5	86.	333	188	.11	.04	.55	2.2	9.0	4.4	71.
	17	51	61	39	7	46	61	56	08	54	19	43	92	71	3	18	33	36
MMI	47.	86.	210	228	103	108	152	515	141	55.	106	183	334	639	149	377	706	193
DFA2	143	700	.12	.17	4.2	4.2	4.8	7.8	39.	908	.31	.85	.71	.28	9.7	2.3	0.3	11.
	06	28	54	81	61	79	93	49	99	86	09	68	55	1	91	19	8	52
MMF	63.	107	276	606	264	232	534	149	312	114	153	289	838	154	299	111	192	393
A2	672	.05	.25	.57	0.9	4.8	0.3	94.	34.	.88	.35	.38	.47	3.2	9.6	12.	69.	98.
	87	44	31	85	13	82	14	2	65	96	08	37	38	63	33	15	14	9
MGM	60.	101	260	485	203	191	365	104	220	113	155	294	683	125	254	573	104	249
FA2	156	.21	.26	.61	3.1	0.1	2.8	35.	38.	.05	.65	.04	.36	3.3	9.9	3.5	79.	14.
	58	36	49	54	64	15	06	71	59	64	62	38	42	04	69	75	77	38
MHM	62.	99.	267	666	318	245	578	164	353	124	159	306	985	177	334	135	224	479
FA2	086	483	.47	.63	5.7	9.0	0.9	65.	78.	.25	.72	.65	.27	5.2	3.2	07.	43.	24.
	43	76	46	09	94	28	43	6	11	06	58	53	93	03	44	94	45	32
MMI	37.	61.	170	350	167	142	277	853	204	70.	100	200	559	107	213	754	132	297
NFA1	333	899	.78	.76	8.8	7.3	3.2	7.9	23.	788	.50	.11	.17	3.8	3.7	0.6	10.	93.
	23	06	38	49	96	29	87	59	32	18	95	85	27	92	42	51	54	78
MMA	24.	46.	123	203	975	101	148	506	140	37.	62.	129	308	611	142	374	702	192
XFA1	206	355	.99	.16	.31	3.6	5.4	0.5	34.	339	140	.78	.53	.04	7.6	6.3	9.1	32.
	15	86	5	22	42	3	99	24	66	87	81	88	39	02	38	46	77	9
MMI	24.	47.	125	203	976	101	148	506	140	37.	63.	130	308	611	142	374	702	192
DFA1	682	358	.76	.47	.02	4.5	6.0	1.8	36.	606	027	.69	.87	.41	8.5	6.7	9.6	34.
	04	69	85	09	94	12	12	03	08	75	02	96	46	88	97	15	23	02
MMF	30.	60.	153		115	126	221	672	163	49.	77.	154	379	753	168	473	903	217
AI	315	742	.36	266	2.7	9.2	2.9	6.7	05.	633	566	.05	.49	.87	3.2	9.4	3.6	65.
	26	21	14	.62	83	23	11	37	33	28	78	86	58	93	15	85	43	92
MGM	27.	52.	137	218	102	106	156	525	143	48.	80.	158	331	651	150	380	713	194
FA1	522	237	.30	.32	5.3	0.6	2.1	7.8	25.	058	506	.35	.74	.83	2.5	8.8	8.8	25.
	57	84	46	19	53	99	97	85	27	66	8	87	73	53	53	79	97	4
MHM	28.	51.	141	475	271	180	548	158	342	64.	84.	169	833	151	283	133	220	471
FA1	320	104	.70	.80	0.6	7.3	8.7	30.	02.	810	458	.69	.83	4.3	6.8	28.	84.	86.
	67	98	67	2	43	02	18	91.	56	82	95	98	03	38	53	72	64	75
MM	66.	107	282	647	306	238	554	157	338	124	163	313	952	172	324	129	216	460
MINF	878	.26	.76	.27	1.9	8.0	3.3	85.	91.	.80	.30	.65	.53	0.5	0.7	92.	17.	76.
A2	53	41	14	7	03	59	08	5	13	26	37	15	94	76	07	7	43	27
MM	37.	69.	150	166	604	435	121	318	555	40.	73.	100	250	357	621	290	410	
MAX	110	409	.96	.99	.03	.41	5.1	1.9	3.4	341	538	.36	.68	.73	.37	2.3	5.0	702
FA2	85	64	5	68	19	48	67	94	56	64	01	62	56	67	44	69	44	2.9



Global Journal of Engineering Science and Research Management

MM	45.	82.	190	181	640	490	123	324	562	49.	94.	135	266	375	681	412	707	
MID	464	846	.40	.06	.78	.69	9.6	0.2	7.5	944	588	.33	.37	.65	.24	291	2.6	8.7
FA2	94	71	92	97	82	53	49	06	45	67	92	56	01	98	68	6.2	87	01
MM	63.	106	274	603	259	231	533	149	307	114	152	284	832	151	294	110	190	378
MFA	486	.82	.82	.92	2.2	1.0	4.9	30.	21.	.41	.17	.88	.30	9.2	5.7	12.	08.	00.
2	56	27	54	47	8	75	64	81	13	12	19	06	81	33	95	43	7	9
MMG	59.	100	255	471	186	177	357	969	179	112	154	290	663	116	233	511	833	162
MFA	736	.31	.95	.41	6.1	4.7	6.4	9.6	41.	.47	.76	.55	.87	6.2	2.9	7.3	9.4	67.
2	71	61	27	32	68	82	15	97	07	65	29	9	92	38	49	05	68	55
MMH	61.	98.	264	666	318	245	578	164	353	124	159	305	985	177	334	135	224	479
MFA	860	343	.73	.58	5.7	8.3	0.9	65.	78.	.17	.30	.45	.26	5.1	3.0	07.	43.	24.
2	75	19	19	06	4	5	4	58	07	36	58	32	37	58	38	94	45	31
MM	34.	50.	134	319	142	104	263	739	154	66.	87.	160	525	938	170	712	117	239
MINF	579	575	.78	.03	9.2	2.0	6.0	6.2	67.	541	070	.10	.26	.78	7.5	7.2	26.	02.
A1	24	21	56	86	54	27	17	66	12	39	61	63	31	1	02	57	86	1
MM	20.	29.	68.	154	571	388	119	312	548	29.	36.	53.	236	342	569	288	408	697
MAX	291	894	486	.51	.08	.66	2.2	8.3	4.4	338	285	501	.93	.16	.54	9.3	8.3	0.7
FA1	4	47	76	05	81	74	91	86	85	15	7	91	05	29	78	17	08	97
MM	20.	31.	70.	154	571	389	119	312	548	29.	37.	54.	237	342	570	288	408	697
MID	789	203	802	.82	.92	.80	2.9	9.8	6.3	614	411	729	.28	.58	.89	9.6	8.7	2.2
FA1	41	24	62	13	73	11	12	3	56	02	49	29	81	08	78	95	94	98
MM	26.	49.	109	223	782	786	202	516	898	42.	56.	89.	318	523	983	399	653	111
MFA	852	031	.66	.74	.85	.69	3.3	0.9	2.9	916	753	524	.70	.68	.90	6.5	7.3	00.
1	57	99	25	66	5	69	11	92	78	19	32	82	22	61	25	69	08	01
MMG	23.	37.	86.	170	630	454	128	335	589	41.	60.	96.	262	391	685	295	421	724
MFA	820	669	692	.38	.20	.95	3.9	7.8	2.0	153	682	127	.93	.37	.72	4.7	1.3	2.9
1	22	62	28	7	23	3	78	96	68	14	5	92	57	14	36	72	21	87
MMH	24.	36.	93.	462	267	162	548	158	341	59.	65.	114	826	149	274	133	220	471
MFA	835	194	204	.10	6.6	7.0	5.3	18.	57.	620	795	.24	.48	0.4	3.0	27.	81.	72.
1	7	92	48	27	25	75	81	58	46	3	28	06	05	03	33	95	08	74
SMIN	66.	107	282	648	306	238	555	158	339	125	163	313	954	172	324	130	216	461
FA2	980	.44	.98	.58	6.6	9.9	2.8	08.	12.	.01	.51	.85	.97	2.9	2.6	21.	44.	08.
FA2	79	56	15	98	58	62	94	04	74	19	14	7	17	4	58	02	25	73
SMA	41.	74.	164	280	112	.17	9.3	6.2	4.1	577	055	.72	.11	.73	.65	8.0	7.2	13.
XFA2	82	09	49	91	5	98	06	05	78	66	44	08	85	31	89	38	82	63
SMID	48.	86.	198	290	115	739	213	577	902	67.	107	157	421	644	101	564	754	126
FA2	560	073	.85	.99	3.7	.89	7.6	4.5	1.1	419	.09	.11	.47	.71	9.6	8.5	2.4	64.
FA2	83	95	18	4	36	56	63	04	23	04	85	94	12	37	4	04	11	54
SMF	63.	107	275	610	265	231	536	150	308	115	153	286	853	154	296	113	193	385
A2	876	.03	.36	.33	4.3	6.2	3.0	23.	91.	.89	.45	.78	.45	4.5	3.4	96.	09.	12.
A2	95	26	99	41	37	76	36	37	91	16	91	75	19	45	94	05	41	34
SGM	60.	101	257	504	207	182	391	106	194	114	155	292	719	125	241	717	107	203
FA2	568	.10	.67	.16	7.4	9.7	1.0	86.	63.	.27	.73	.02	.79	4.5	1.8	2.1	58.	70.
FA2	93	33	34	72	42	83	75	29	95	32	89	71	72	65	35	17	77	09
SHM	62.	99.	265	666	318	245	578	164	353	124	159	305	985	177	334	135	224	479
FA2	375	321	.74	.72	5.8	8.5	0.9	65.	78.	.40	.73	.92	.32	5.2	3.1	07.	43.	24.
FA2	52	73	03	66	18	75	55	6	09	27	93	92	5	15	03	94	45	32
SMIN	39.	59.	150	391	174	120	318	891	173	79.	101	177	613	107	187	857	133	267
FA1	665	744	.58	.13	6.8	3.1	5.0	1.1	36.	270	.34	.99	.03	4.8	1.9	4.7	78.	13.
FA1	37	18	64	64	51	19	88	23	86	8	47	55	3	68	11	44	13	82
SMA	27.	43.	92.	270	109	650	210	568	889	52.	62.	87.	399	618	925	562	751	125
XFA1	862	189	920	.75	8.4	.47	2.0	0.5	0.9	443	640	671	.93	.15	.21	8.0	2.7	65.
XFA1	62	18	73	58	42	79	94	85	32	5	72	4	14	14	26	51	94	58
SMID	28.	44.	95.	271	109	651	210	568	889	52.	63.	88.	400	618	926	562	751	125
FA1	289	236	017	.00	9.1	.52	2.5	1.8	2.6	667	546	778	.20	.49	.40	8.3	3.2	66.
FA1	95	75	44	6	38	05	62	34	63	68	44	86	36	88	13	42	17	98
SMF	33.	58.	128	322	126	989	272	723	118	62.	78.	118	459	756	126	640	939	160
A1	349	505	.94	.18	2.2	.12	2.3	1.5	56.	417	356	.58	.22	.56	8.4	0.2	3.7	68.
A1	16	8	29	41	25	19	44	29	68	54	17	85	68	74	05	38	49	86
SGM	30.	49.	109	283	114	709	217	586	925	61.	81.	124	418	656	102	567	761	128
FA1	840	408	.04	.02	5.5	.16	0.8	9.5	4.7	158	327	.15	.99	.76	3.3	7.2	6.7	11.
FA1	71	91	63	09	15	3	09	88	46	39	39	33	39	72	51	02	07	97



Global Journal of Engineering Science and Research Management

SHM	31.	48.	114	495	272	169	549	158	341	74.	84.	139	846	151	277	133	471
FAI	583	194	.49	.71	2.3	8.1	8.6	38.	72.	124	835	.08	.84	7.3	7.5	31.	220
FAI	54	67	87	59	07	35	67	48	01	33	26	14	84	23	55	21	86
LTSM	67.	107	283	650	307	239	556	158	340	125	163	314	957	172	324	130	216
INFA	112	.75	.70	.35	4.2	6.3	4.0	43.	17.	.33	.81	.48	.75	6.8	8.9	56.	94.
2	49	31	32	57	61	52	63	24	54	83	75	79	07	35	35	78	41
LTSM	46.	81.	191	350	162	118	289	802	169	75.	105	173	555	890	153	721	110
AXFA	490	358	.67	.47	3.4	0.6	9.6	1.9	28.	164	.29	.93	.42	.80	1.8	4.3	58.
2	95	69	16	65	19	75	63	02	76	5	4	91	01	03	77	76	01
LTSM	51.	89.	216	358	164	121		805	169	80.	117	194	563	900	156	722	110
IDFA	812	999	.85	.66	3.9	3.3	291	9.3	74.	243	.47	.42	.97	.77	7.2	2.1	68.
2	94	42	5	13	34	24	3.7	78	95	74	02	66	62	62	67	96	79
LTSM	64.	107	277	617	273	233	539	151	315	117	154	291	875	157	300	117	197
FA2	340	.38	.01	.03	1.2	2.3	3.4	49.	45.	.61	.94	.34	.42	5.4	7.6	03.	28.
2	47	29	37	38	7	16	11	75	7	23	43	63	85	28	74	52	79
LTSG	61.	102	262	528	230	195	421	117	236	116	156	295	776	134	257	836	133
MFA	510	.23	.23	.77	0.3	7.8	7.3	01.	33.	.29	.91	.66	.86	6.7	2.0	6.7	20.
2	96	67	56	85	33	22	3	4	77	13	31	02	32	81	68	07	61
LTSH	63.	100	268	666	318	245	578	164	353	124	160	307	985	177	334	135	224
MFA	015	.74	.89	.97	5.9	9.4	0.9	65.	78.	.76	.45	.33	.42	5.3	3.3	07.	43.
2	84	18	69	27	66	73	77	64	16	36	59	28	11	43	52	95	46
LTSM	44.	69.	181	437	206	152	367	103	222	89.	113	209	701	121	217	945	152
INFA	893	791	.57	.50	4.1	4.8	5.4	80.	71.	118	.06	.24	.27	0.8	1.8	5.0	14.
1	1	36	57	28	51	7	86	48.	1	75	11	26	58	49	83	03	67
LTSM	35.	57.	140	342	160	115	288	798	168	69.	84.	146	547	881	149	720	110
AXFA	603	353	.08	.93	4.4	1.6	6.3	6.1	84.	153	491	.45	.52	.67	9.7	6.9	47.
1	86	83	22	08	42	91	33	84	67	85	7	93	37	35	24	02	66
LTSM	35.	58.	141	343	160	115	288	798	168	69.	85.	147		881	150	720	110
IDFA	952	149	.63	.12	4.9	2.4	6.6	7.1	85.	318	156	.24	547	.92	0.6	7.1	47.
1	57	85	51	59	39	25	99	77	88	56	52	08	.74	88	02	2	96
LTSM	39.	68.	166	382	172	138	333	914	188	76.	95.	167	591	979	174	778	123
FAI	979	860	.03	.99	1.1	1.2	9.1	6.1	06.	528	908	.65	.76	.64	1.7	2.0	55.
4	42	45	08	91	04	74	75	45	04	48	99	82	31	22	26	95	47
LTSG	38.	62.	151	352	163	119	293	813	171	75.	98.	171	562	909	156	724	111
MFA	000	040	.79	.46	8.0	2.3	8.7	2.4	33.	594	085	.48	.12	.31	9.8	3.5	21.
1	33	43	15	64	67	39	07	9	2	71	51	17	19	1	8	95	36
LTSH	38.	61.	155	522	278	185	551	158	342	85.	101	182	868	155	285	133	471
MFA	503	123	.78	.57	1.5	9.8	5.1	69.	39.	269	.34	.27	.21	2.8	6.9	36.	220
1	46	93	11	45	59	74	88	18	1	27	28	74	47	12	66	64	97
LMS	67.	107	283	650	307	239	556	158	340	125	163	314	958	172	325	130	217
MINF	168	.83	.89	.80	5.6	7.3	5.7	53.	33.	.43	.96	.67	.17	8.6	1.8	62.	10.
A2	74	37	85	44	33	34	99	33	86	99	87	43	57	54	22	11	29
LMS	48.		196	374	169	122	299	834	176	78.	110	185	581	966	163	746	116
MAX	126	82.	.17	.29	7.1	3.3	0.4	3.8	74.	373	.86	.17	.34	.21	2.1	1.7	91.
FA2	54	502	95	18	67	43	14	97	94	81	5	3	46	35	97	45	97
LMS	52.	90.	220	381	171	125		837	177	83.	121	203	589	975	166	746	117
MID	991	750	.07	.90	6.4	4.7	300	7.6	18.	166	.77	.94	.25	.71	4.8	9.4	01.
FA2	88	47	76	45	72	2	3.6	71	27	45	55	07	13	49	99	5	92
LMS	64.	107	277	618	274	233	539	151	316	118	155	292	877	158	302	117	198
MFA	531	.47	.42	.94	3.4	4.3	8.0	78.	30.	.07	.64	.61	.95	9.6	2.4	46.	35.
2	66	35	45	94	31	61	69	79	01	74	51	91	87	3	29	22	75
LMS	61.	102	263	537	233	196	425	118	240	116	157	296	784	138	261	856	138
GMF	888	.49	.24	.25	3.4	8.0	9.1	57.	33.	.83	.47	.68	.46	6.7	0.5	6.1	31.
A2	75	27	59	4	66	55	69	19	42	11	17	02	31	91	41	67	47
LMS	63.	101	269	667	318	245	578	164	353	124	160	307	985		334	135	224
HMF	233	.04	.62	.03	6.0	9.6	0.9	65.	78.	.87	.73	.70	.46	177	3.4	07.	43.
A2	58	71	33	26	01	61	8	66	17	4	14	33	62	5.4	75	95	47
LMS	46.	71.	186	454	211	155	373	105	227	91.	117	217	714	126	223	960	316
MINF	662	486	.59	.17	1.1	0.3	7.7	87.	30.	488	.82	.40	.48	5.6	0.7	2.4	156
A1	17	08	96	97	18	06	31	23	11	01	83	57	56	33	9	15	05
LMS	38.	59.	147	367	167	119	297	831	176	72.	92.	159	574	957	160	745	116
MAX	116	600	.20	.17	9.3	4.7	7.9	2.0	33.	665	131	.40	.03	.62	2.2	4.3	82.
FA1	79	37	09	42	66	71	75	67	52	15	84	26	17	3	41	59	42



Global Journal of Engineering Science and Research Management

LMS	38.	60.	148	367	167	119	297	831	176	72.	160	574	957	160	745	116	220	
MID	436	369	.67	.36	9.8	5.5	8.3	2.9	34.	825	92.	.14	.23	.86	3.0	4.5	82.	74.
FA1	48	27	71	07	3	11	15	41	66	67	726	74	17	11	66	75	7	25
LMS	42.	70.	171	404		141	341	940	194	79.	102	179	614	105	182	800	129	243
MFA	145	599	.85	.33	178	3.7	3.2	2.8	36.	661	.42	.36	.72	1.4	6.1	7.3	20.	69.
1	55	8	02	43	9.2	39	11	28	48	84	17	07	65	09	87	32	03	58
LMS	40.		158	376	171	123	302	844	178	78.	104	182	587	983	166	749	117	222
GMF	321	64.	.32	.14	0.9	4.6	7.2	4.3	66.	780	.38	.90	.54	.88	7.3	0.4	50.	44.
A1	94	099	7	9	48	11	59	51	48	28	35	27	05	96	1	35	67	89
LMS	40.	63.	162	529	279	187	551	158	342	87.	106	191	872	156	287	133	221	472
HMF	709	222	.12	.91	2.3	5.8	7.4	79.	51.	759	.97	.93	.47	3.8	7.6	37.	00.	00.
A1	18	06	74	51	7	52	61	87	29	05	83	48	04	62	99	97	65	61
LAD	66.	107	282	646	305	238	553	157	338	124	163	313	951	171	323	129	215	460
MINF	792	.10	.48	.50	8.8	6.2	7.0	69.	62.	.65	.16	.46	.18	9.0	7.8	98.	42.	
A2	64	49	35	2	97	68	88	05	41	85	03	97	44	55	45	03	04	36
LAD	27.	60.	118	12.	21.	27.	28.	32.	19.	13.	49.	55.	15.	9.8	28.	60.	28.	17.
MAX	662	092	.65	666	321	059	076	156	413	869	878	344	819	527	549	059	117	319
FA2	18	83	65	96	7	19	18	6	81	92	97	33	56	45	96	06	63	05
LAD	40.	78.	172	28.	52.	77.	40.	58.	40.	27.	79.	100	33.	24.	81.	66.	32.	31.
MID	069	265	.70	265	764	326	502	489	711	198	005	.99	207	579	688	074	922	987
FA2	84	67	73	45	17	02	59	11	37	84	96	08	58	29	06	06	77	81
LAD	63.	106	274	599	253	230	531	148	304	113	151	282	812	149	291	107	187	369
MFA	092	.63	.08	.20	9.7	5.8	4.2	53.	61.	.15	.11	.87	.31	5.9	6.6	17.	15.	15.
2	87	63	82	42	28	67	64	06	18	54	79	85	59	92	28	28	11	33
LAD	58.	99.	253	436	163	170	315	846	149	110	153	289	590	105	218	281	510	103
GMF	757	491	.28	.51	6.0	1.1	3.9	7.1	10.	.90	.98	.06	.99	8.0	2.7	1.7	1.0	59.
A2	14	09	97	43	73	32	08	28	22	74	98	09	96	22	12	72	75	31
LAD	61.	96.	262	666	318	245	578	164	353	124	158	304	985	177	334	135	224	479
HMF	019	803	.46	.49	5.6	8.1	0.9	65.	78.	.00	.90	.89	.23	5.1	2.9	07.	43.	24.
A2	39	39	81	59	95	13	33	57	06	7	54	42	63	26	66	94	44	31
LAD		32.	95.	223	105	774	184	534	116	50.	68.	133	395	756	137	558	955	198
MINF	23.	411	510	.66	2.2	.01	6.8	5.0	84.	673	707	.03	.15	.52	6.6	1.9	4.9	64.
A1	717	88	06	09	11	13	12	79	41	55	67	39	23	17	98	59	26	
LAD	1.4	2.2	2.9	3.2	3.3	1.5	19.	14.	5.7	0.9	1.2	0.9	5.1	2.1	1.3	55.	24.	8.3
MAX	890	705	313	778	711	283	290	975	287	110	022	463	239	125	457	355	538	036
FA1	15	44	48	4	5	81	98	16	53	3	65	14	01	93	5	24	81	95
LAD	2.1	3.9		3.4	3.8	2.1	19.	15.	6.7	1.0	2.1	1.7	5.3	2.2	1.8	55.	24.	8.7
MID	045	342	5.6	558	354	810	671	933	878	907	483	560	066	598	114	515	691	850
FA1	97	68	502	81	67	61	9	44	44	72	17	35	38	56	43	96	47	69
LAD	11.	30.	58.	85.	209	438	979	227	339	17.	26.	41.	101	201	435	130	275	412
MFA	328	067	916	370	.25	.00	.14	3.2	1.2	387	399	327	.62	.11	.98	5.8	6.5	6.4
1	32	46	42	15	6	66	76	12	89	21	16	13	09	7	45	11	14	23
LAD	6.5	12.	25.	16.	42.	43.	70.	134	173	14.	31.	49.	29.	40.	86.	88.	73.	103
GMF	022	921	988	109	947	169	577	.43	.76	971	862	843	158	108	142	129	164	.09
A1	73	07	78	97	56	3	7	75	67	91	21	17	23	92	09	72	72	74
LAD	6.8	8.6	29.	425	263	152	547	158	341	41.	37.	70.	808	146	269	133	220	471
HMF	734	055	328	.26	9.3	1.1	6.8	04.	39.	125	800	169	.82	7.3	4.8	26.	78.	68.
A1	22	51	18	74	82	28	21	31	87	52	2	83	51	73	1	41	06	14

Table 6: AMSE of the estimators when $n = 40$ and $\sigma_{outlier}^2$ (magnitude of outliers) = 250

ESTI MAT ORS	NUMBER OF EXPLANATORY VARIABLES																				
	3									5											
	DEGREES OF MULTICOLLINEARITY									DEGREES OF MULTICOLLINEARITY											
	0.900			0.990			0.999			0.900			0.990			0.999					
	% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS					
	10	20		10	20		10	20	10	20		10	20		10	20		10	20		
	5%	%	%	5%	%	%	5%	%	%	5%	%	%	5%	%	%	5%	%	%	5%	%	%
OLS	374	982	204	559	109	186	665	108	157	465	929	221	549	128	227	685	174	326			
	.05	.47	1.2	7.8	61.	87.	09.	120	058	.81	.93	8.0	7.3	17.	23.	55.	245	077			
	49	39	34	08	25	53	36	.6	.7	16	51	28	19	35	94	5	.9	.3			
MMI	359	942	195	535	105	179	636	103	150	449	897	213	530	123	219	661	167	314			
NFA2	.06	.44	9.5	9.0	00.	24.	84.	651	630	.18	.21	9.8	0.3	27.	14.	21.	861	194			
	95	58	47	71	79	49	43	.6	.2	17	81	84	78	37	72	81	.9	.5			



Global Journal of Engineering Science and Research Management

MMA	205	449	115	176	357	733	195	352	192	494	115	162	422	939	199	558		
XFA2	.63	.02	3.9	3.6	6.0	4.5	61.	22.	610	.14	.75	4.8	0.6	5.9	3.0	25.	01.	135
	22	54	65	93	9	06	22	85	38	64	65	19	35	11	56	54	42	762
MMI	246	531	133	186	377	763	196	354	613	228	588	131	172	435	974	199	559	135
DFA2	.22	.29	0.8	1.6	6.2	9.4	62.	74.	38.	.53	.49	5.4	0.1	3.7	0.0	92.	49.	937
	77	62	36	25	87	57	98	09	24	83	9	82	38	55	63	79	44	.4
MMF	336	889	185	476	987	167	546	944	140	418	840	197	477	106	199	599	147	275
A2	.40	.52	8.0	3.5	7.6	74.	66.	48.	880	.22	.89	2.2	3.4	33.	26.	03.	919	609
	28	04	27	87	12	41	99	91	.2	55	56	42	39	93	63	6	.9	.2
MGM	319	811	174	381	790	137	355	652	100	421	858	199	394	843	167	328	819	173
FA2	.09	.19	3.0	8.0	4.2	31.	37.	25.	132	.31	.69	9.8	6.0	7.6	06.	01.	60.	323
	92	11	87	57	9	44	49	65	.6	74	62	23	72	59	26	29	15	.5
MHM	328	887	185	554	108	184	664	108	156	435	869	209	546	127	225	685	174	325
FA2	.77	.71	3.6	5.1	43.	67.	61.	011	830	.11	.04	0.5	3.1	46.	85.	20.	169	937
	08	45	13	01	59	94	22	.4	.7	55	82	4	23	07	69	42	.3	.7
MMI	199	530	119	286	568	105	346	581	896	266	544	138	309	746	142	394	101	206
NFA1	.31	.04	5.0	8.2	3.9	54.	93.	71.	07.	.13	.91	6.2	3.0	7.7	29.	99.	423	265
	49	12	93	9	69	44	17	05	18	53	59	34	58	31	54	78	.2	.2
MMA	127	342	854	167	339	705	194	349	607	145	325	914	153	411	906	198	556	135
XFA1	.29	.65	.70	4.0	1.7	1.2	65.	89.	53.	.48	.45	.21	1.4	0.0	9.2	61.	60.	593
	85	78	56	65	71	43	54	18	09	86	55	49	22	14	04	64	06	.4
MMI	129	345	863	167	339	705	194	349	607	146	330	921	153	411	907	198	556	135
DFA1	.67	.33	.47	6.3	6.5	8.5	68.	95.	60.	.77	.72	.54	3.7	3.1	8.0	63.	64.	598
	54	84	2	18	46	93	15	51	9	46	24	5	89	83	27	5	18	.3
MMF	155	423	100	201	440	851	233	428	726	193	412	107	203	503	108	265	689	154
A1	.31	.17	6.6	5.7	6.7	0.5	07.	73.	05.	.54	.14	9.1	0.8	2.2	12.	81.	77.	442
	97	52	22	79	06	2	83	78	79	01	56	46	58	64	57	01	37	.5
MGM	143	377	932	177	362	741	200	360	622	197		110	169	438	958	202	564	
FA1	.92	.55	.49	7.9	5.8	0.1	56.	89.	08.	.25	436	4.3	1.8	6.8	9.1	50.	74.	136
	69	33	32	74	7	19	24	59	39	42	.96	82	69	08	05	1	43	789
MHM	146	413	985	431	822	140	648	104	149	207	435	117	459	109		673	171	321
FA1	.76	.63	.17	0.8	2.4	14.	04.	343	481	.05	.46	7.2	0.3	22.	192	63.	638	359
	26	8	34	72	37	07	81	.4	.6	49	98	72	33	61	81	77	.4	.9
MM	358	941	195	535	104	178	636	103	150	448	896	213	529	123	218	660	167	
MINF	.89	.42	5.5	5.9	88.	92.	38.	530	310	.96	.23	5.8	7.6	12.	72.	77.	717	313
A2	17	88	18	85	96	43	2	.1	.4	15	79	98	35	66	89	42	.9	524
MM	195	398	851	138	206	306	147	218	244	170	417	743	127	264	376	143	326	456
MAX	.26	.13	.95	1.1	6.7	34.	51.	50.	.13	.11	.91	2.2	9.3	1.4	24.	71.	15.	
FA2	79	77	88	9	24	44	13	92	71	45	76	83	49	39	42	1	01	04
MM	239	490	111	150	231	350	148	221	248	210	534	995	138	280	429	143	328	458
MID	.12	.16	8.2	6.0	0.3	2.7	43.	48.	36.	.33	.34	.20	3.3	6.9	0.9	99.	45.	57.
FA2	53	71	82	05	69	37	07	59	72	2	24	92	08	22	16	7	48	59
MM	335	885	183	473	981	165	540	934	139	416	834	193	474	104	194	594	145	265
MFA	.43	.47	9.1	3.5	8.3	85.	65.	99.	078	.76	.81	7.7	6.1	29.	89.	91.	964	295
2	6	25	8	32	65	98	93	99	.3	32	17	24	17	95	68	07	.2	.1
MMG	317	800	169	371	753	126	326	586	834	420	854	197	385	782	150	290	662	106
MFA	.23	.75	6.5	2.8	0.2	32.	92.	86.	93.	.01	.59	2.0	4.3	9.0	25.	97.	30.	601
2	66	53	83	43	78	46	14	71	55	56	74	74	11	03	57	57	96	.1
MMH	327	883	183	554	108	184	664	108	156	434	866	208	546	127	225	685	174	325
MFA	.53	.73	6.1	4.8	42.	65.	61.	011	830	.54	.38	1.8	3.0	45.	84.	20.	169	937
2	59	11	06	89	83	3	21	.4	.3	53	78	99	49	79	69	41	.3	.6
MM	188	488	914	266	476	795	317	499	676	251	480	110	291	665	112	367	906	160
MINF	.45	.76	.19	1.4	3.1	3.2	33.	25.	10.	.81	.13	4.3	7.8	4.1	97.	46.	38.	266
A1	86	36	58	84	77	73	04	04	82	44	57	13	14	94	65	36	87	.9
MM	111	278	413	128	184	268	146	215	240	119	200	367	117	251	329	142	325	453
MAX	.98	.92	.93	3.1	4.0	9.4	32.	75.	94.	.26	.28	.65	4.6	0.0	8.4	52.	05.	84.
FA1	77	94	44	51	91	56	3	82	06	24	28	86	26	16	09	42	95	58
MM	114	281	425	128	184	269	146	215	241	120	206	378	117	251	331	142	325	453
MID	.50	.96	.58	5.8	9.4	8.6	35.	83.	03.	.59	.98	.12	7.1	3.7	0.0	54.	10.	91.
FA1	15	07	09	03	1	1	07	3	69	44	97	05	62	38	95	5	74	28
MM	141	369	630	168	311	480	188	310	414	171	311	624	173	365	597	219	495	754
MFA	.44	.22	.43	7.6	9.0	9.7	64.	08.	49.	.67	.88	.23	2.8	5.4	1.7	52.	47.	67.
1	07	04	03	66	79	59	14	91	57	34	92	77	58	44	97	35	43	3



Global Journal of Engineering Science and Research Management

MMG	129	318	521	140	212	317	152	228	259	175	343	664	135	284		146	470
MFA	.44	.15	.98	6.5	2.2	2.9	68.	75.	98.	.77	.68	.21	1.6	7.9	405	90.	334
I	29	93	16	98	87	07	2	36	88	49	05	63	46	78	8.5	02	75
MMH	133	359	606	423	792	130	647		149	186	341	781	455	107	187	673	171
MFA	.05	.25	.68	5.9	0.9	5.5	89.	104	080	.76	.67	.65	4.8	84.	49.	55.	613
I	08	58	7	8	83	08	17	266	.3	81	11	78	68	99	38	27	.9
SMIN	359	942	195	536	105	179	637	103	150	449	897	213	530	123	218	661	167
FA2	.42	.92	7.1	6.2	04.	05.	34.	700	414	.74	.49	7.4	7.0	26.	91.	68.	924
	68	07	23	29	98	95	63	.1	.5	83	25	29	57	02	2	84	.4
SMA	223	486	983	220	370	505	224	379	395	235	516	928	227	440	662	260	589
XFA2	.82	.11	.78	6.8	7.9	6.7	57.	81.	77.	.67	.92	.26	1.7	2.1	0.4	91.	33.
	39	99	82	21	79	76	63	48	11	11	29	2	39	17	09	54	6
SMID	258	561		229	390	542	225	382	399	264	604	113	235	452	705	261	590
FA2	.47	.14	121	5.2	4.8	9.8	50.	24.	30.	.31	.21	8.7	2.5	3.6	5.6	50.	73.
	42	56	0.5	25	34	93	71	76	98	05	74	62	13	44	14	3	16
SMF	338	891	184	482	989	166	551	947		421	842	195	483	106	196	603	148
A2	.16	.81	6.8	1.1	2.8	67.	37.	27.	139	.48	.53	1.8	5.0	32.	89.	62.	406
	34	7	91	06	02	91	78	13	721	07	46	7	1	73	76	31	.9
SGM	322	817	171	399	796	131	370	665	903	424	859	198	414	846	158	369	841
FA2	.38	.74	6.0	3.3	0.1	32.	90.	08.	87.	.24	.80	3.3	2.0	6.8	32.	67.	21.
	39	75	08	48	12	5	55	97	82	11	28	51	83	58	14	02	.8
SHM	330	889	184	554	108	184	664	108	156	436	869	208	546	127	225	685	174
FA2	.76	.54	3.0	5.4	43.	66.	61.	011	830	.60	.69	5.1	3.3	46.	85.	20.	169
	96	32	6	32	92	35	24	.5	.4	78	02	85	14	07	13	43	.3
SMIN	218	560	103	317	578	915	362	597	768	294	563	123	345	752	127	426	103
FA1	.45	.00	6.6	6.0	3.7	8.5	97.	31.	17.	.21	.66	0.3	2.0	1.4	38.	17.	021
	11	64	95	08	33	41	8	96	6	79	67	36	51	28	32	48	.7
SMA	156	385	605	212	352	472	223	377	392	198	356	609	219	429	622	260	588
XFA1	.41	.36	.31	5.6	8.9	6.4	69.	52.	47.	.97	.28	.38	7.9	2.4	0.7	35.	00.
	42	45	73	84	56	39	81	48	83	77	34	84	82	74	57	57	36
SMID	158	388	615	212	353	473	223	377	392	199	361	618	219	429	623	260	588
FA1	.51	.05	.84	7.7	3.5	4.6	71.	59.	56.	.99	.39	.70	9.9	5.4	1.4	37.	04.
	98	44	75	17	32	5	81	04	42	8	45	52	77	67	69	2	45
SMF	180	462	794	243	452	653	258	451	544	236	439	827	260	517	841	317	715
A1	.87	.25	.75	3.1	7.0	1.2	01.	85.	75.	.76	.33	.90	2.1	2.0	1.9	35.	78.
	63	93	63	01	25	74	69	7	99	45	48	5	05	1	07	38	72
SGM	171	419	700	221	375	514	229	388	409	239	462	861	232	455	686	263	595
FA1	.01	.40	.99	9.7	6.8	8.1	05.	13.	84.	.67	.75	.45	9.6	5.1	5.8	73.	69.
	5	99	68	46	04	58	87	67	1	91	67	45	46	2	27	88	85
SHM	172	452	771	440	827	134	648	104	149	247	459	957	466	109	190	673	171
FA1	.99	.17	.27	6.0	0.6	79.	25.	376	208	.54	.43	.27	6.4	33.	00.	75.	647
	69	33	62	7	89	11	78	.6	.1	21	45	26	74	74	14	03	.6
LTSM	360	944	196	538	105	179	639	103	150	450	899	214	531	123	219	663	168
INFA	.24	.97	2.1	1.6	33.	49.	10.	963	795	.87	.58	1.6	8.5	59.	42.	20.	331
2	77	4	19	5	83	97	93	.1	.9	46	86	17	92	83	07	2	.8
LTSM	252	568	123	287	542	851	330	548	687	286	598	124	299	635	104	348	843
AXFA	.01	.14	5.4	5.9	0.0	4.9	94.	24.	76.	.18	.70	1.8	8.9	8.1	94.	67.	40.
2	74	82	43	31	88	69	01	01	76	3	21	33	39	92	9	42	66
LTSM	278	627	139	294	556	877	331	550	690	307	664	138	305	644	108	349	844
IDFA	.36	.10	2.9	5.2	0.2	8.0	61.	00.	47.	.30	.69	7.0	6.6	8.4	01.	13.	49.
2	78	98	8	14	33	77	37	95	4	07	53	55	88	27	26	07	3
LTSM	341	899	186	491	100	168	568	963		427	852	198	491	109	200	613	152
FA2	.74	.52	7.6	8.6	09.	86.	25.	21.	141	.08	.47	3.6	8.0	75.	89.	63.	036
	19	66	05	68	67	66	87	45	631	05	83	11	17	8	87	44	.9
LTSG	328	836	176	425	850	141	434	749	104	429	866	200	437	933	171	430	103
MFA	.65	.36	2.8	6.6	3.7	61.	92.	94.	502	.32	.94	9.2	1.9	9.6	23.	15.	336
2	32	1	19	87	82	03	29	21	.9	91	54	75	17	88	58	22	.8
LTSH	335	897	186	554	108	184	664	108		439	875	209	546	127	225	685	174
MFA	.14	.89	4.1	6.4	46.	70.	61.	011	156	.27	.01	4.3	3.7	46.	86.	20.	169
2	08	06	74	31	26	58	31	.7	831	76	6	27	58	89	68	48	.4
LTSM	247	626		362	691	113	429	701	949	329	633	145	385	864	148	473	117
INFA	.95	.20	127	3.7	0.1	43.	26.	72.	34.	.47	.90	0.7	2.1	2.3	52.	16.	423
1	59	4	2	01	62	42	64	9	76	99	37	94	16	98	77	46	.2



Global Journal of Engineering Science and Research Management

LTSM	200	492	974	281	529	827	330	546	685	259	479	102	294	627	102	348	842	143
AXFA	.57	.80	.28	1.2	4.0	3.1	29.	56.	21.	.16	.16	0.9	5.3	4.5	11.	23.	36.	961
1	28	99	68	31	58	22	95	59	13	27	86	67	71	57	33	76	83	.7
LTSM	202	494	981	281	529	827	330	546	685	259	483	102	294	627		348	842	143
IDFA	.25	.71	.56	2.8	7.2	9.3	31.	61.	28.	.92	.05	7.7	6.8	6.8	102	25.	39.	966
1	29	57	79	81	43	45	7	25	12	06	59	19	44	91	19	03	86	.2
LTSM	219	549	110	305	600	953	354	599	793	286	540	117	323	692	117	390	939	161
FA1	.52	.78	5.2	2.3	5.8	8.2	78.	46.	82.	.98	.90	2.9	4.5	1.8	57.	92.	34.	629
	31	1	09	14	38	04	85	55	2	75	02	3	01	08	1	08	47	.8
LTSG	211	517	104	288	545	857	334	554	698	289	558	119	304	647	106	350	848	145
MFA	.98	.50	0.5	6.1	4.7	9.9	17.	26.	36.	.13	.27	5.9	0.3	1.6	67.	85.	34.	072
1	07	26	12	09	59	97	1	7	4	26	55	6	8	02	75	43	14	.6
LTSH	213	543	108	457	872	144	648	104	149	294	556	125	477	111	194	674		321
MFA	.26	.84	8.1	5.9	5.1	03.	94.	558	685	.80	.56	9.2	8.7	85.	99.	15.	171	405
1	26	56	3	22	02	34	13	.9	.3	11	57	53	96	12	52	96	724	.8
LMS	360	945	196	538	105	179	639	104	150	451	900	214	532	123	219	663	168	314
MINF	.27	.99	3.1	5.3	39.	55.	83.	063	867	.46	.45	2.8	4.3	67.	62.	82.	370	723
A2	32	68	49	37	52	75	43	.8	.2	18	36	07	36	5	78	38	.2	.2
LMS	251	606	128	309	582	880	350	555	739	300	625	126	324	660	114	374	851	159
MAX	.52	.13	4.1	4.9	5.6	3.2	85.	01.	45.	.74	.58	5.3	3.2	5.3	94.	12.	31.	361
FA2	01	71	41	56	81	26	53	71	15	42	82	48	11	96	38	96	58	.9
LMS	278	659	142	315	595	905	351	556	741	320	684	140		669	117	374	852	159
MID	.02	.26	7.5	5.0	8.0	5.1	50.	84.	93.	.06	.78	6.4	329	0.9	73.	54.	30.	511
FA2	95	59	1	85	43	64	42	42	49	35	04	15	5.1	67	19	32	71	.1
LMS	341	903	187	494	100	169	573	966	141	429	856	198	495	110	202	617	152	280
MFA	.74	.30	1.5	4.8	34.	12.	16.	63.	976	.31	.04	9.2	1.3	28.	26.	11.	084	336
2	88	19	25	39	36	89	4	6	.1	38	27	66	66	77	5	17	.9	.1
LMS	328	845	177	433	863	142	449	757	106	431	869	201	445	945	175	447	102	191
GMF	.60	.52	1.4	3.0	2.7	59.	55.	17.	842	.39	.57	4.1	8.2	2.0	02.	63.	776	600
A2	58	59	88	38	64	56	27	59	.3	18	67	94	16	62	97	28	.3	.6
LMS	335	901	186	554	108	184	664	108	156	440	876	209	546	127	225	685	174	325
HMF	.28	.04	8.1	6.7	46.	71.	61.	011	831	.44	.92	6.6	4.0	47.	87.	20.	169	937
A2	84	86	98	43	7	24	36	.8	.1	98	4	06	06	12	33	5	.4	.8
LMS	247	658	131	375	719	115	444	709	979	340	657	146	399	878	154	486	116	220
MINF	.43	.45	7.2	7.5	0.1	28.	29.	30.	32.	.28	.13	8.6	8.6	1.2	35.	92.	765	103
A1	07	79	71	92	77	04	55	88	24	01	28	41	85	97	8	83	.4	.3
LMS	199	534	104	303	570	857	350	553	737	276	518	105	319	652	112	373	850	159
MAX	.66	.93	8.1	8.4	3.7	3.0	24.	28.	09.	.04	.23	4.2	4.9	5.9	33.	73.	36.	218
FA1	14	6	71	49	41	42	06	3	81	93	1	84	75	5	01	38	67	.6
LMS	201	536	105	303	570	857	350	553	737	276	521	106	319	652	112	373	850	159
MID	.34	.82	4.9	9.9	6.8	8.9	25.	33.	16.	.73	.75	0.5	6.3	8.1	40.	74.	39.	222
FA1	31	48	44	07	86	31	74	09	25	51	42	44	02	69	17	54	44	.8
LMS	218	589	116	324	637	978	374	607	836	301	573	119	345	713	126	412	938	175
MFA	.75	.25	6.6	8.4	0.0	5.7	02.	01.	02.	.48	.82	8.8	3.8	9.1	36.	15.	63.	345
1	68	71	95	38	33	89	79	59	21	13	64	69	97	49	52	54	97	.3
LMS	211	558	110	310	585	886	353	561	749	303	589	122	328	671	116	376	855	160
GMF	.14	.94	8.5	3.7	8.6	5.4	98.	21.	14.	.44	.39	1.0	0.4	2.9	51.	10.	80.	236
A1	13	98	04	91	44	04	26	88	5	61	32	51	63	27	95	29	61	.1
LMS	212	581	115	462	882	145	649	104	149	308	587	128	482	112	196	674	171	321
HMF	.33	.27	2.1	8.2	0.4	05.	23.	627	775	.09	.26	4.2	1.2	30.	57.	31.	736	445
A1	3	44	34	2	16	32	64	.6	.7	64	63	87	96	1	99	85	.6	.5
LAD	358	939	195	534	104	178	635	103	150	448	895	213	529	122	218	660		313
MINF	.43	.87	3.9	8.8	79.	79.	52.	401	185	.41	.44	4.4	1.7	99.	58.	08.	167	321
A2	86	19	43	33	39	62	85	.7	.5	74	63	74	74	1	53	21	562	.2
LAD	141	174	593	80.	125	220	52.	73.	68.	67.	287	445	66.	71.	280	35.	28.	24.
MAX	.05	.80	.40	258	.33	.63	549	599	622	129	.58	.70	988	489	.94	565	801	115
FA2	76	23	52	2	37	02	41	76	52	18	66	67	99	64	76	32	58	72
LAD	207	324	956	208	359	627	90.	179	174	128	450	771	185	211	793	52.	61.	56.
MID	.64	.07	.81	.68	.20	.93	261	.70	.81	.03	.44	.91	.05	.22	.32	368	280	077
FA2	99	2	45	96	17	62	09	62	02	94	45	29	64	38	66	56	1	89
LAD	332	877	183	464	976	164	526	923	138	412	828	192	467	101	192	586	143	260
MFA	.62	.39	0.6	8.0	4.5	99.	00.	27.	228	.50	.82	2.2	4.7	58.	97.	54.	347	979
2	12	11	3	35	38	9	83	53	.3	34	44	49	99	61	42	33	.5	.3



Global Journal of Engineering Science and Research Management

LAD	311	774	167	333	709	119	236	480	715	416	850	196	356	680	140	184	403	678
GMF	.29	.36	2.2	9.1	4.7	85.	29.	20.	57.	.27	.78	0.0	2.5	0.8	66.	99.	11.	29.
A2	18	22	93	8	72	73	8	59	09	54	13	27	88	29	55	69	33	76
LAD	321	874	182	554	108	184	664	108	156	432	863	207	546	127	225	685	174	325
HMF	.35	.33	3.7	4.5	42.	64.	61.	011	830	.85	.62	7.9	2.9	45.	84.	20.	169	937
A2	01	03	51	38	22	26	18	.3	.2	65	44	32	01	57	37	4	.3	.6
LAD	130	321	679	183	350	615	222	359	509	190	375	912	229	520	942	290	729	134
MINF	.18	.82	.81	9.8	8.9	1.0	48.	30.	60.	.30	.73	.75	4.0	3.7	3.4	66.	19.	529
A1	03	5	74	43	57	18	15	01	33	91	31	1	98	71	89	72	87	.8
LAD	4.0	3.5	11.	4.3	4.6	7.3	28.	11.	8.5		4.1	5.6	3.8	2.4	5.0	24.	9.8	4.3
MAX	654	069	003	658	531	698	555	867	032	1.3	324	032	979	064	308	609	749	784
FA1	86	42	04	42	99	23	44	56	33	413	44	17	01	64	32	1	13	53
LAD	7.5	6.4	23.	6.1	7.5	13.	30.	17.	14.	2.2	9.5	12.	4.9	3.6	9.2	25.	11.	6.3
MID	553	368	002	139	945	028	190	144	223	208	680	970	336	812	549	244	237	754
FA1	19	53	54	83	07	3	52	48	97	21	69	46	66	61	24	45	46	06
LAD	51.	127	282	441	132	214	436	992	172	69.	139	291	639	122	274	869	182	298
MFA	564	.99	.87	.22	7.5	6.6	4.5	4.9	60.	440	.97	.85	.23	3.8	4.6	8.4	99.	06.
1	19	05	11	67	83	66	43	65	28	85	23	92	18	43	08	64	27	15
LAD	31.	49.	135	97.	176	309	346	609	751	75.	184	342	148	253	555	169	290	430
GMF	129	570	.82	167	.49	.57	.90	.48	.33	619	.27	.92	.79	.08	.39	.43	.18	.51
A1	81	86	28	7	6	56	86	92	69	58	68	23	07	56	3	71	51	42
LAD	26.	96.	207	404	758	124	647	104	148	88.	174	476	446	106	185	673	171	321
HMF	169	203	.75	0.1	1.1	94.	61.	184	923	834	.04	.07	1.8	23.	10.	43.	593	242
A1	47	36	1	22	6	45	17	.5	.3	94	26	84	65	98	92	17	.4	.3

Table 7: AMSE of the estimators when n = 100 and $\sigma^2_{outlier}$ (magnitude of outliers) = 10

ESTI MAT ORS	NUMBER OF EXPLANATORY VARIABLES																	
	3									5								
	DEGREES OF MULTICOLLINEARITY									DEGREES OF MULTICOLLINEARITY								
	0.900			0.990			0.999			0.900			0.990			0.999		
	% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS		
5%	10	20	5%	10	20	5%	10	20	5%	10	20	5%	10	20	5%	10	20	
OLS	0.4	0.5	1.2	2.9	5.9	14.	38.	58.	155	0.3	0.6	1.5	4.5	8.6	16.	51.	80.	186
	395	856	936	889	513	205	319	301	.29	557	942	581	261	650	040	072	212	.22
	32	25	93	69	19	16	08	65	95	97	43	13	78	79	88	22	77	18
MMI NFA2	0.4	0.5	1.2	2.9	5.8	13.	37.	57.	152	0.3	0.6	1.5	4.4	8.5	15.	50.	79.	183
	324	762	730	398	555	975	676	349	.71	508	848	368	632	396	823	359	074	.48
	64	57	79	41	88	41	25	68	56	3	28	74	87	79	42	76	51	41
MMA XFA2	0.2	0.4	0.9	1.2	2.5	6.2	13.	20.	62.	0.2	0.4	1.0	1.7	3.4	6.8		28.	76.
	885	211	365	869	111	910	151	419	423	543	523	081	692	008	913	18.	277	358
	32	17	3	69	24	79	31	94	68	61	11	47	34	89	67	055	84	95
MMI DFA2	0.3	0.4	1.0	1.4	2.7	6.8	13.	20.	63.	0.2	0.5	1.1	1.9	3.6	7.3	18.	28.	76.
	296	730	452	686	989	867	337	781	194	868	190	479	206	917	699	221	516	783
	28	59	07	44	56	31	65	44	59	16	32	7	08	3	67	86	42	77
MMF A2	0.4	0.5	1.2	2.8	5.7	13.	36.	55.	148	0.3	0.6	1.4	4.2	8.0	15.	47.	75.	172
	246	685	497	757	043	569	508	986	.17	442	675	947	792	828	343	992	543	.07
	08	22	43	57	16	22	13	62	2	39	67	18	37	98	25	4	02	47
MGM FA2	0.4	0.5	1.2	2.6	5.1	12.	29.	45.	120	0.3	0.6	1.5	4.0	7.5	14.	35.	57.	129
	083	509	130	328	733	284	012	614	.38	491	775	156	127	683	399	924	554	.69
	96	22	28	24	62	94	14	63	76	64	01	22	83	79	7	22	3	95
MHM FA2	0.4	0.5	1.1	2.9	5.8	14.	38.	58.	155	0.3	0.6		4.5	8.6	15.	51.	80.	186
	051	300	810	514	835	072	275	227	.14	340	554	1.4	013	171	955	048	167	.12
	35	11	33	89	61	01	96	81	96	39	79	781	72	98	16	31	13	98
MMI NFA1	0.2	0.3	0.7	1.6	3.3	8.1	20.	31.	89.	0.2	0.4	0.9	2.7	5.2	10.	31.	48.	117
	595	468	935	434	530	930	650	829	463	153	260	833	377	389	014	056	112	.00
	67	39	77	02	74	88	81	83	31	6	13	36	7	9	42	84	89	39
MMA XFA1	0.1	0.2	0.6	1.0	2.1	5.6	12.	20.	61.	0.1	0.2	0.6	1.6	3.0	6.4	17.	28.	75.
	926	598	015	833	996	567	975	082	686	465	748	709	142	930	056	896	050	951
	93	71	97	72	85	19	22	62	21	59	62	01	59	81	54	85	4	17
MMI DFA1	0.1	0.2	0.6	1.0	2.2	5.6	12.	20.	61.	0.1	0.2	0.6	1.6	3.0	6.4	17.	28.	75.
	940	625	074	852	026	627	12.	085	693	484	777	761	157	960	103	898	052	955
	33	47	66	63	6	73	977	99	71	39	12	31	45	6	99	49	77	43



Global Journal of Engineering Science and Research Management

MMF A1	0.2 267 07	0.3 102 3	0.6 986 44	1.3 498 02	2.7 051 82	6.6 835 04	16. 042 23	25. 496 83	73. 083 59	0.1 796 58	0.3 396 7	0.7 985 49	2.0 005 04	3.7 432 67	7.8 570 98	22. 189 97	34. 691 68	87. 003 23
MGM FA1	0.2 074 21	0.2 825 39	0.6 499 07	1.1 519 31	2.3 285 28	5.9 244 06	13. 337 32	20. 701 88	63. 112 6	0.2 016 61	0.3 738 97	0.8 563 55	1.7 793 21	3.3 985 48	6.9 546 28	18. 318 35	28. 756 79	77. 182 27
MHM FA1	0.2 047 86	0.2 708 96	0.6 281 02	1.7 358 27	3.5 795 01	9.1 480 82	34. 804 05	52. 408 6	143 .06 46	0.1 605 31	0.3 083 66	0.7 476 04	3.2 490 56	6.2 123 01	11. 787 78	48. 976 45	76. 270 13	178 .28 31
MM MINF A2	0.4 324 07	0.5 761 6	1.2 726 93	2.9 394 49	5.8 544 52	13. 972 1	37. 671 06	57. 340 56	152 .67 34	0.3 507 96	0.6 847 27	1.5 365 11	4.4 628 06	8.5 382 58	15. 819 62	50. 353 79	79. 062 26	183 .43 39
MM MAX FA2	0.2 706 65	0.4 014 52	0.8 622 72	1.0 621 52	1.8 105 71	4.0 846 48	9.6 808 74	13. 897 17	31. 854 77	0.2 464 18	0.4 152 84	0.8 610 37	1.3 786 97	2.3 407 38	3.9 938 18	13. 414 36	17. 591 56	37. 359 29
MM MID FA2	0.3 191 9	0.4 626 36	1.0 049 6	1.2 776 53	2.1 734 79	4.9 326 7	9.8 908 78	14. 328 75	32. 870 72	0.2 825 9	0.4 966 99	1.0 575 5	1.5 610 72	2.7 013 78	4.6 886 7	13. 608 41	17. 869 09	37. 912 87
MM MFA 2	0.4 243 59	0.5 682 08	1.2 480 79	2.8 737 75	5.6 972 27	13. 545 29	36. 469 38	55. 935 79	147 .86 46	0.3 440 68	0.6 668 08	1.4 917 11	4.2 726 18	8.0 555 65	15. 308 4	47. 896 93	75. 356 21	170 .86 21
MMG MFA 2	0.4 073 68	0.5 496 99	1.2 077 88	2.6 159 97	5.1 136 6	12. 094 69	28. 258 61	44. 467 55	114 .28 74	0.3 491 04	0.6 771 9	1.5 142 26	3.9 877 1	7.4 810 54	14. 231 34	34. 437 72	54. 426 82	114 .80 1
MMH MFA 2	0.4 038 47	0.5 271 36	1.1 716 62	2.9 512 76	5.8 830 17	14. 070 87	38. 275 94	58. 227 75	155 .14 94	0.3 334 68	0.6 542 04	1.4 740 99	4.5 013 11	8.6 170 4	15. 954 69	51. 048 31	80. 167 11	186 .12 97
MM MINF A1	0.2 360 48	0.3 122 58	0.6 690 91	1.4 847 51	2.8 837 53	6.7 772 09	18. 534 49	27. 945 52	71. 129 59	0.2 021 68	0.3 829 33	0.8 254 17	2.5 358 98	4.6 481 65	8.4 976 78	28. 782 78	42. 671 47	96. 339 92
MM MAX FA1	0.1 607 73	0.2 146 72	0.4 309 64	0.8 287 45	1.4 463 98	3.2 246 68	9.4 861 44	13. 5	30. 922 16	0.1 249 63	0.2 032 77	0.3 807 79	1.1 966 06	1.9 766 18	3.3 316 04	13. 231 99	17. 333 08	36. 841 41
MM MID FA1	0.1 619 89	0.2 171 3	0.4 367 52	0.8 307 18	1.4 494 26	3.2 319 58	9.4 880 86	13. 503 94	30. 931 39	0.1 268 88	0.2 061 81	0.3 871 55	1.1 982 68	1.9 798 64	3.3 374 23	13. 233 86	17. 335 73	36. 846 74
MM MFA 1	0.1 972 41	0.2 689 08	0.5 438 13	1.1 365 62	2.0 542 31	4.6 428 31	13. 064 36	20. 118 52	47. 046 57	0.1 614 17	0.2 774 65	0.5 571 8	1.6 574 62	2.7 657 89	5.4 021 47	18. 323 13	25. 616 59	52. 415 14
MMG MFA 1	0.1 755 63	0.2 376	0.4 837	0.9 044 61	1.5 894 11	3.5 731 37	9.8 904 97	14. 233 37	32. 761 12	0.1 865 17	0.3 189 65	0.6 411 78	1.3 908 04	2.3 378 68	4.0 846 47	13. 721 18	18. 153 64	38. 442 09
MMH MFA 1	0.1 734 69	0.2 262 01	0.4 621 23	1.5 958 99	3.1 864 55	8.0 647 22	34. 681 67	52. 138 34	142 .27 84	0.1 398 45	0.2 414 63	0.4 846 17	3.1 376 31	5.9 119 91	10. 967 21	48. 940 55	76. 163 5	177 .97 12
SMIN FA2	0.4 325 14	0.5 762 87	1.2 728 48	2.9 403 87	5.8 564 93	13. 974 27	37. 684 59	57. 359 59	152 .70 03	0.3 509 02	0.6 849 17	1.5 367 87	4.4 643 1	8.5 408 53	15. 822 59	50. 368 96	79. 084 81	183 .47 75
SMA XFA2	0.2 944 14	0.4 224 71	0.8 929 73	1.4 229 99	2.6 820 85	5.3 504 16	15. 543 39	22. 915 88	48. 864 16	0.2 652 39	0.4 646 37	0.9 606 78	2.1 077 54	3.8 169 71	6.2 822 53	21. 793 56	30. 876 11	66. 062 32
SMID FA2	0.3 337 84	0.4 741 53	1.0 216 29	1.5 856 56	2.9 585 61	6.0 673 63	15. 705 41	23. 252 16	49. 716 23	0.2 930 56	0.5 273 19	1.1 197 82	2.2 371 35	4.0 715 54	6.8 071 65	21. 933 08	31. 096 29	66. 497 45
SMF A2	0.4 248 04	0.5 686 1	1.2 487 59	2.8 781 69	5.7 094 66	13. 560 85	36. 562 98	56. 037 17	148 .05 64	0.3 445 76	0.6 681 22	1.4 939 7	4.2 905 84	8.1 001 04	15. 335 98	48. 114 05	75. 662 22	171 .86 07
SGM FA2	0.4 090 86	0.5 511 98	1.2 099 49	2.6 483 79	5.2 065 03	12. 215 65	29. 706 66	46. 362 07	117 .81 59	0.3 492 86	0.6 777 5	1.5 152 82	4.0 488 18	7.6 140 16	14. 366 28	37. 218 34	58. 560 81	126 .16 95
SHM FA2	0.4 055 47	0.5 302 74	1.1 755 66	2.9 517 92	5.8 838 71	14. 071 56	38. 227 276	58. 227 86	155 .14 95	0.3 349 43	0.6 563 49	1.4 770 25	4.5 015 03	8.6 173 68	15. 955 06	51. 048 32	80. 167 14	186 .12 98



Global Journal of Engineering Science and Research Management

SMIN	0.2	0.3	0.7	1.7	3.4	7.6	22.	33.	81.	0.2	0.4	0.9	2.9	5.4	9.7	32.	49.	111
FAI	666	486	208	433	912	198	206	643	300	324	401	321	383	597	066	937	581	.88
SMA	0.2	0.2	0.5	1.2	2.3	4.6	15.	22.	48.	0.1	0.3	0.5	1.9	3.5	5.7	21.	30.	65.
XFAI	096	702	092	469	999	136	391	606	073	785	085	797	775	537	653	661	666	655
SMID	0.2	0.2	0.5	1.2	2.4	4.6	15.	22.	48.	0.1	0.3	0.5	1.9	3.5	5.7	21.	30.	65.
FAI	102	719	142	484	022	200	392	609	081	797	105	849	787	561	702	663	669	659
SMF	0.2	0.3	0.6	1.4	2.8	5.8	18.	27.	61.	0.2	0.3	0.7	2.3	4.1	7.3	25.	36.	77.
A1	358	130	093	790	681	228	092	709	404	032	617	193	056	169	443	289	875	852
SGM	0.2	0.2	0.5	1.3	2.5	4.9	15.	23.	49.	0.2	0.3	0.7	2.1	3.8	6.3	22.	31.	66.
FAI	193	876	557	044	111	145	705	177	624	211	923	856	163	149	512	013	318	913
SHM	0.2	0.2	0.5	1.8	3.6	8.6	34.	52.	142	0.1	0.3	0.6	3.3	6.3	11.	49.	76.	178
FAI	182	791	366	272	864	895	966	612	.75	882	355	621	726	714	616	037	347	.23
LTSM	0.4	0.5	1.2	2.9	5.8	13.	37.	57.	152	0.3	0.6	1.5	4.4	8.5	15.	50.	79.	183
INFA	326	765	735	422	594	981	712	384	.77	510	851	373	657	434	827	387	110	.55
2	67	97	37	24	44	21	92	85	27	1	14	03	67	33	7	75	14	51
LTSM	0.3	0.4	0.9	1.7	3.3	7.4	21.	30.	73.	0.2	0.4	1.0	2.4	4.5	8.1	27.	40.	93.
AXFA	102	560	783	731	368	187	730	061	304	769	976	741	820	907	046	353	981	716
2	86	4	08	72	35	43	64	33	02	97	38	17	41	36	71	92	33	83
LTSM	0.3	0.4	1.0	1.8	3.5	7.9	21.	30.	73.	0.2	0.5	1.1	2.5	4.7	8.5	27.	41.	94.
IDFA	444	936	708	933	467	190	839	316	933	999	483	941	848	903	045	467	145	039
2	95	45	45	62	71	74	68	09	15	92	32	62	35	87	62	22	79	27
LTSM	0.4	0.5	1.2	2.8	5.7	13.	36.	56.	148	0.3	0.6	1.4	4.3	8.1	15.	48.	75.	173
FA2	253	695	514	859	247	603	726	157	.50	450	693	977	043	364	376	334	75.	.22
2	67	33	95	09	01	54	25	38	96	35	18	17	6	33	54	23	958	4
LTSG	0.4	0.5	1.2	2.6	5.2	12.	31.	47.	123	0.3	0.6	1.5	4.0	7.7	14.	39.	61.	137
MFA	109	543	178	942	957	473	478	990	.80	494	782	171	885	095	527	469	855	.27
2	24	08	33	19	79	83	24	57	93	66	95	29	99	34	24	27	5	17
LTSH	0.4	0.5	1.1	2.9	5.8	14.	38.	58.	155	0.3	0.6	1.4	4.5	8.6	15.	51.	80.	186
MFA	077	368	888	527	852	073	276	228	.14	362	585	819	017	177	955	048	167	.12
2	22	09	23	69	37	82	15	04	98	08	37	82	22	39	8	34	18	99
LTSM	0.2	0.4	0.8	2.0	3.9	9.0	26.	38.	96.	0.2	0.4	1.0	3.1	5.9	10.	36.	54.	126
INFA	861	045	591	098	511	168	239	054	573	504	781	528	497	049	743	151	937	.64
1	65	23	05	07	49	74	53	31	49	74	34	83	68	18	6	96	19	67
LTSM	0.2	0.3	0.7	1.6	3.1	6.8	21.	29.	72.	0.2	0.3	0.7	2.3	4.3	7.7	27.	40.	93.
AXFA	361	525	146	438	159	915	627	821	709	070	743	944	774	820	069	246	824	410
1	38	13	39	18	15	88	95	9	68	63	45	87	25	49	57	53	55	53
LTSM	0.2	0.3	0.7	1.6	3.1	6.8	21.	29.	72.	0.2	0.3	0.7	2.3	4.3	7.7	27.	40.	93.
IDFA	366	535	180	449	3.1	965	628	824	715	080	760	983	784	840	107	247	826	413
1	61	01	72	07	179	05	98	31	67	54	25	59	22	7	44	64	18	71
LTSM	0.2	0.3	0.7	1.8	3.4	7.7	23.	33.	82.	0.2	0.4	0.8	2.6	4.8	8.9	30.	45.	102
FA1	592	803	831	145	782	482	445	607	293	270	164	964	392	260	144	158	421	.09
2	52	13	82	67	63	65	54	48	49	65	41	83	85	91	98	26	84	
LTSG	0.2	0.3	0.7	1.6	3.2	7.1	21.	30.	73.	0.2	0.4	0.9	2.4	4.5	8.1	27.	41.	94.
MFA	445	634	465	856	053	122	839	260	865	413	404	448	888	891	572	532	311	344
1	73	53	35	77	12	16	49	13	93	8	07	81	76	41	67	73	49	08
LTSH	0.2	0.3	0.7	2.0	4.0	9.8	35.	53.	143	0.2	0.3	0.8	3.5	6.6	12.	49.	76.	178
MFA	435	582	331	653	916	087	394	173	.85	151	964	547	143	622	270	131	550	.69
1	11	45	56	14	88	62	15	18	48	09	33	21	53	87	46	96	29	04
LMS	0.4	0.5	1.2	2.9	5.8	13.	37.	57.	152	0.3	0.6	1.5	4.4	8.5	15.	50.	79.	183
MINF	326	765	734	419	590	981	704	389	.76	510	851	372	655	433	829	384	114	.55
A2	91	63	87	76	73	86	71	21	18	03	55	75	7	31	14	23	36	13
LMS	0.3	0.4	0.9	1.7	3.2	7.6	21.	31.	72.	0.2	0.5	1.0	2.4	4.4	8.3	26.	40.	91.
MAX	145	509	689	559	886	410	277	196	885	746	026	613	425	993	481	739	870	239
FA2	14	51	43	72	03	02	92	85	25	59	86	59	56	66	9	87	59	34
LMS	0.3	0.4	1.0	1.8	3.4	8.1	21.	31.	73.	0.2	0.5	1.1	2.5	4.7	8.7	26.	41.	91.
MID	472	906	659	771	996	255	390	445	535	989	522	858	473	118	350	854	038	575
FA2	02	87	96	55	4	13	74	11	26	06	21	71	94	94	74	58	05	06



Global Journal of Engineering Science and Research Management

LMS	0.4	0.5	1.2	2.8	5.7	13.	36.	56.	148	0.3	0.6	1.4	4.3	8.1	15.	48.	75.	173
MFA	254	694	512	849	227	608	687	178	.44	450	696	974	032	334	386	298	990	.15
2	65	21	97	27	7	22	72	45	69	12	02	43	52	16	08	46	08	03
LMS	0.4	0.5	1.2	2.6	5.2	12.	31.	48.		0.3	0.6	1.5	4.0	7.7	14.	39.	61.	136
GMF	112	538	172	893	853	505	268	297	123	494	784	170	863	009	559	081	937	.32
A2	84	78	23	33	24	63	71	64	.32	56	18	09	24	22	51	23	14	57
LMS	0.4	0.5	1.1	2.9	5.8	14.	38.	58.	155	0.3	0.6	1.4	4.5	8.6	15.	51.	80.	186
HMF	081	357	877	526	850	073	276	228	.14	360	587	816	016	176	955	048	167	.12
A2	33	79	3	34	85	98	1	05	98	97	71	48	82	91	88	34	19	99
LMS	0.2	0.3	0.8	1.9	3.9	9.1	25.	38.	96.	0.2	0.4	1.0	3.1	5.8	10.	35.	54.	
MINF	915	959	420	944	096	821	928	865	070	463	835	393	297	696	904	615	990	125
A1	69	55	5	58	66	81	67	46	79	11	11	15	6	7	6	74	1	.33
LMS	0.2	0.3	0.6	1.6	3.0	7.1	21.	30.	72.	0.1	0.3	0.7	2.3	4.2	7.9	26.	40.	90.
MAX	450	380	859	255	703	249	172	963	263	998	804	692	368	778	666	630	710	919
FA1	23	62	74	38	75	8	46	01	38	27	26	31	62	12	16	13	78	61
LMS	0.2	0.3	0.6	1.6	3.0	7.1	21.	30.	72.	0.2	0.3	0.7	2.3	4.2	7.9	26.	40.	90.
MID	454	393	897	266	722	298	173	965	269	008	820	733	378	799	702	631	712	922
FA1	94	39	14	21	78	66	52	37	71	62	96	08	61	23	09	28	44	94
LMS	0.2	0.3	0.7	1.7	3.4	7.9	23.	34.	81.	0.2	0.4	0.8	2.6	4.7	9.1	29.	45.	99.
MFA	661	697	602	977	305	604	062	622	927	211	224	765	031	497	325	523	377	908
1	96	67	1	54	89	07	24	98	11	43	21	23	82	61	37	56	52	33
LMS	0.2	0.3	0.7	1.6	3.1	7.3	21.	31.	73.	0.2	0.4	0.9	2.4	4.4	8.3	26.	41.	91.
GMF	526	510	206	676	577	422	390	390	466	365	462	270	495	976	989	920	206	891
A1	61	31	16	01	08	41	54	63	11	43	2	56	03	65	78	56	64	85
LMS	0.2	0.3	0.7	2.0	4.0	9.9	35.	53.	143	0.2	0.4	0.8	3.5	6.6		49.	76.	178
HMF	517	445	056	523	604	208	314	233	.76	085	019	329	007	209	12.	126	567	.65
A1	15	83	65	39	74	09	18	11	67	03	15	06	42	4	337	42	78	51
LAD	0.4	0.5	1.2	2.9	5.8	13.	37.	57.	152	0.3	0.6	1.5	4.4	8.5	15.	50.	79.	183
MINF	323	760	724	392	538	970	668	335	.65	507	846	363	625	374	818	351	055	.41
A2	63	85	89	56	81	51	93	24	45	59	7	59	43	75	22	03	96	48
LAD	0.2	0.3	0.7	0.9	1.3	2.3	7.7	8.5	12.	0.2	0.3	0.7	1.1	1.5	2.1	10.	10.	16.
MAX	549	804	969	035	198	446	029	002	991	370	842	657	038	875	731	899	601	449
FA2	99	5	35	47	4	02	77	71	34	38	91	32	63	69	35	87	15	3
LAD	0.3	0.4	0.9	1.1	1.7	3.4	7.9	8.9	14.	0.2	0.4	1.0	1.3	2.0	3.0	11.	10.	17.
MID	103	524	735	457	514	009	285	728	085	776	794	027	066	033	070	100	905	034
FA2	82	31	93	57	84	44	46	41	2	71	18	28	86	41	89	54	83	69
LAD	0.4	0.5	1.2	2.8	5.6	13.	36.	55.	147	0.3	0.6	1.4	4.2	8.0	15.	47.	75.	170
MFA	241	679	471	727	935	532	452	905	.72	438	663	903	686	392	293	850	256	.35
2	67	58	45	68	23	86	9	12	22	76	51	48	57	8	54	48	04	51
LAD	0.4	0.5	1.2	2.6	5.0	11.	27.	43.	110	0.3	0.6	1.5	3.9	7.4	14.	33.	52.	107
GMF	065	486	045	067	799	978	884	663	.95	490	770	136	714	261	152	684	530	.50
A2	59	77	98	23	7	85	56	09	89	39	09	15	55	14	26	83	77	91
LAD	0.4	0.5	1.1	2.9	5.8	14.	38.	58.	155	0.3	0.6		4.5	8.6	15.	51.	80.	186
HMF	024	234	632	511	826	070	275	227	.14	328	531	1.4	012	169	954	048	167	.12
A2	93	01	81	35	75	3	93	72	94	79	62	72	75	48	5	3	1	97
LAD	0.2	0.2	0.5	1.3	2.5	5.6	17.	24.	59.	0.1	0.3	0.7	2.3	4.2	7.5	27.	39.	85.
MINF	146	703	416	777	830	978	377	896	957	863	457	219	910	427	855	599	279	972
A1	58	07	18	45	66	91	15	03	78	21	69	94	9	54	1	44	98	78
LAD	0.1	0.1	0.2	0.6	0.8	1.3	7.4	8.0	12.	0.0	0.1	0.1	0.9	1.1	1.4	10.	10.	15.
MAX	264	438	080	443	868	098	948	825	032	968	285	673	042	764	148	714	321	920
FA1	5	96	91	12	36	55	77	32	91	81	28	99	26	88	56	49	35	7
LAD	0.1	0.1	0.2	0.6	0.8	1.3	7.4	8.0	12.	0.0	0.1	0.1	0.9	1.1	1.4	10.	10.	15.
MID	277	470	157	464	903	179	969	865	042	990	318	746	060	799	209	716	324	926
FA1	26	47	06	18	32	12	45	47	08	34	83	78	04	7	13	38	2	02
LAD	0.1	0.2	0.3	0.9	1.6	3.0	11.	15.	30.	0.1	0.2	0.3	1.4	2.0	3.8	16.	19.	33.
MFA	687	147	668	871	101	390	385	718	750	389	180	864	141	776	694	212	765	988
1	63	06	81	85	23	1	33	42	01	82	95	92	28	91	8	36	88	81
LAD	0.1	0.1	0.2	0.7	1.0	1.7	7.9	8.8	13.	0.1	0.2	0.4	1.1	1.5	2.2	11.	11.	17.
GMF	431	738	812	271	555	176	281	672	965	681	686	925	172	842	812	218	221	608
A1	19	04	58	47	78	75	37	1	38	9	32	29	88	7	87	35	44	33
LAD	0.1	0.1	0.2	1.4	2.9	7.2	34.	51.	141	0.1	0.1	0.2	3.0	5.7	10.	48.	76.	177
HMF	403	578	465	960	132	766	621	962	.90	138	734	922	634	108	519	922	106	.84
A1	97	06	08	65	94	45	96	44	04	81	47	51	95	59	65	29	75	63



Global Journal of Engineering Science and Research Management

Table 8: AMSE of the estimators when $n = 100$ and $\sigma_{outlier}^2$ (magnitude of outliers) = 100

ESTI MAT ORS	NUMBER OF EXPLANATORY VARIABLES																		
	3									5									
	DEGREES OF MULTICOLLINEARITY									DEGREES OF MULTICOLLINEARITY									
	0.900			0.990			0.999			0.900			0.990			0.999			
	% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS			
	5%	10	20	5%	10	20	5%	10	20	5%	10	20	5%	10	20	5%	10	20	
OLS	25.	52.	137	305	609	110	417	554	120	35.	71.	132	349	676	147	424	861	154	
	808	308	.33	.86	.77	3.9	1.1	5.4	33.	005	069	.40	.39	.97	9.6	3.1	0.6	16.	
	84	96	68	19	93	38	71	09	18	69	27	01	51	34	34	58	68	05	
MMI	25.	51.	135	300	599	108	394	545	118	34.	70.	130	344	667	145	418	848	151	
	392	438	.08	.81	.59	5.8	410	4.0	33.	520	076	.57	.54	.58	9.0	1.6	5.9	99.	
	51	92	47	82	59	57	0.8	15	06	82	21	26	1	47	42	36	65	33	
MMA	16.	37.	95.	86.	196	461	105	165	435	20.	40.	82.	106	230	588	261	581		
	683	928	366	526	.61	.52	9.0	2.8	9.7	167	855	394	.71	.90	.49	115	4.7	0.1	
	77	97	27	39	24	49	11	88	71	66	22	12	66	35	49	3.8	36	02	
MMI	19.	42.	108	99.	227	506	108	169	442	24.	48.	95.	122	256	627	116	263	585	
	452	851	.86	492	.50	.85	1.0	3.1	5.0	329	725	226	.03	.32	.89	9.1	7.3	3.1	
	88	63	62	01	1	11	57	49	26	97	58	48	31	86	32	63	98	3	
MMF	24.	50.	132	289	583	106	394	532	116	33.	68.	126	332	640	140	396	800	145	
	710	875	.24	.99	.44	7.1	5.5	8.2	66.	625	521	.13	.63	.90	9.4	9.9	3.3	98.	
	18	49	37	76	83	42	49	35	69	05	87	24	45	69	28	25	38	81	
MGM	23.	49.	128	254	520	962	303	431	956	34.	69.	128	313	606	131	284	571	112	
	895	347	.26	.32	.28	.80	9.1	4.9	4.1	116	276	.66	.73	.83	4.5	9.0	7.0	07.	
	52	45	11	92	4	67	86	1	69	57	84	57	7	37	86	3	65	38	
MHM	23.	46.	125	302	602	109	416	553	120	33.	67.	125	347	672	147	424	860	154	
	256	707	.89	.76	.99	0.4	7.7	8.3	19.	073	207	.00	.30	.79	1.1	0.9	6.4	07.	
	85	93	76	3	52	96	99	79	07	13	38	87	13	28	28	77	13	76	
MMI	14.	28.	76.	149	303	617	203	286	656	19.	40.	80.	192	387	898	235	493	947	
	007	575	256	.29	.66	.83	7.7	3.3	8.4	170	481	789	.01	.67	.21	2.6	6.9	4.0	
	16	68	69	11	39	42	52	11	7	68	79	47	88	09	45	32	7	71	
MMA	9.5	19.	52.	73.	165	416	103	161	429	10.	23.	51.	91.	205	549	113	259	576	
	966	978	197	901	.69	.24	8.6	5.7	8.3	224	483	250	572	.47	.44	9.4	3.2	9.2	
	33	03	25	37	06	87	94	13	52	69	91	54	38	9	38	03	42	52	
MMI	9.6	20.	52.	74.	165	416	103	161	429	10.	23.	51.	91.	205	549	113	259	576	
	899	265	886	013	.96	.66	8.8	6.0	8.9	355	702	707	709	.71	.82	9.5	3.4	9.6	
	34	89	86	07	47	84	96	82	71	3	26	33	59	96	17	51	65	76	
MMF	11.	25.	63.	101	225	524	139	220	563	13.	31.	61.	129	267	682	151	708		
	314	374	492	.49	.20	.01	4.5	6.7	8.8	929	291	835	.19	.26	.96	7.0	326	1.4	
	16	97	86	44	59	4	53	64	28	72	65	84	12	3	01	35	7.8	54	
MGM	10.	22.	57.	80.	179	438	108	168	442	15.	34.	68.	107	234	599	117	266	589	
	473	310	912	438	.38	.01	1.2	2.2	3.7	836	294	620	.66	.37	.67	6.6	0.0	5.4	
	31	08	95	69	21	99	62	63	61	96	69	24	07	52	43	53	74	24	
MHM	10.	20.	55.	171	339	656	387	497	109	12.	27.	57.	236	462	105	405	823	147	
	149	853	878	.65	.31	.13	7.2	3.3	04.	320	535	615	.48	.90	9.5	0.4	5.7	02.	
	04	49	97	35	46	07	1	77	18	74	48	29	54	81	15	57	01	16	
MM	25.	51.	135	300	599	108	410	545	118	34.	70.	130	344	667	145	418	848	151	
	390	430	.05	.80	.54	5.5	0.4	3.0	29.	519	066	.54	.51	.50	8.6	1.2	4.7	94.	
	86	73	66	36	24	17	89	89	4	33	85	07	84	35	78	28	92	77	
MM	16.	36.	88.	75.	155	240	856	994	182	19.	36.	69.	84.	159	282	783	161	208	
	258	587	617	830	.80	.24	.54	.86	9.8	442	684	329	516	.11	.47	.49	7.1	9.2	
	68	89	94	52	26	06	46	59	69	24	3	89	11	27	19	94	39	24	
MM	19.	42.	105	89.	190	307	880	103	191	23.	46.	87.	101	190	340	800	164	214	
	208	172	.39	606	.30	.33	.22	9.1	2.9	900	071	079	.58	.16	.39	.28	2.9	5.4	
	FA2	86	9	19	78	42	05	29	74	52	56	63	74	41	61	49	47	81	35
MM	24.	50.	132	289	583	106	394	532	116	33.	68.	125	332	639	140	396	797	145	
	699	853	.10	.86	.11	5.7	2.6	3.2	54.	613	464	.79	.38	.83	5.5	2.8	9.2	39.	
	36	91	45	58	08	84	76	38	81	88	2	04	66	27	49	51	39	18	
MMG	23.	49.	127	253	517	945	299	419	914	34.	69.	128	312	603	129	272	536	100	
	864	261	.83	.22	.00	.66	1.5	4.3	8.7	111	247	.53	.73	.22	5.8	6.9	1.4	72.	
	2	97	87	83	26	46	67	33	94	63	76	39	82	13	28	19	41	74	
MMH	23.	46.	125	302	602	109	416	553	120	33.	67.	124	347	672	147	424	860	154	
	200	446	.30	.75	.97	0.3	7.7	8.3	19.	051	103	.61	.29	.77	1.0	0.9	6.4	07.	
	2	24	27	89	74	19	22	99	75	05	95	09	7	78	92	77	12	75	



Global Journal of Engineering Science and Research Management

MM	13.	25.	64.	142	276	472	191	244	498	18.	36.	67.	179	350	739	215	442	752
MINF	395	793	113	.59	.70	.49	3.0	3.2	5.0	368	236	071	179	.00	.00	8.0	6.2	1.7
AI	11	51	51	16	9	56	25	73	22	68	73	98	.89	27	27	1	14	97
MM	8.6	16.	34.	62.	122	176	834	955	175	8.7	16.	25.	67.	129	228	768	159	203
MAX	876	027	205	386	.50	.46	.67	.13	4.7	112	091	001	872	.40	.79	.02	3.0	7.5
FA1	59	41	52	75	09	41	73	9	66	29	43	77	12	21	52	04	86	8
MM	8.7	16.	35.	62.	122	177	834	955	175	8.8		25.	68.	129	229	768	159	203
MID	873	348	006	506	.78	.00	.89	.52	5.5	499	16.	611	019	.66	.26	.17	3.3	8.1
FA1	31	19	33	73	16	88	47	53	04	23	337	19	78	1	38	79	33	06
MM	10.	22.	47.	91.	187	332	121	164	362	12.	25.	40.	109	203	422	119	240	393
MFA	516	114	861	735	.72	.93	7.2	2.3	9.4	703	232	004	.58	.59	.61	6.0	3.1	4.6
I	68	78	31	65	08	31	28	74	67	99	81	18	73	13	68	55	43	73
MMG	9.6	18.	40.	69.	136	206	880	102	191	14.	28.	49.	85.	163	298	808		220
MFA	211	635	983	361	.96	.29	.44	7.0	1.3	768	819	757	564	.32	.73	.54	166	2.0
I	09	33	14	71	73	74	25	93	16	16	93	4	53	32	24	03	9.2	35
MMH	9.2	17.	38.	166	317	530	387	494	108	10.	20.	33.	229	440	969	404	822	146
MFA	838	029	768	.39	.92	.62	2.9	7.5	13.	953	864	901	.74	.00	.07	7.5	7.9	68.
I	44	48	43	85	61	79	95	51	55	82	76	97	74	53	01	48	56	39
SMIN	25.	51.	135	300	599	108	410	545	118	34.	70.	130	344	667	145	418	848	151
FA2	399	442	.07	.90	.71	5.6	1.5	4.5	31.	530	084	.56	.61	.65	8.9	2.8	7.9	97.
	62	98	56	86	42	85	55	59	39	89	39	45	01	9	35	62	6	74
SMA	17.	38.	93.	133	251	363	141	190	351	22.	43.	78.	152	269	511	179	353	492
XFA2	940	503	337	.85	.57	.03	0.8	9.0	4.7	943	381	999	.06	.23	.85	8.6	1.3	8.6
	12	65	84	31	38	52	49	34	78	93	41	86	85	56	57	44	77	28
SMID	20.	43.	107	143	276	417	142	194		26.	50.	93.	163	291	555	181	355	497
FA2	213	145	.79	.46	.85	.83	9.2	5.5	358	125	348	099	.48	.36	.70	0.2	0.7	3.9
	73	6	85	08	79	75	36	28	6.4	11	26	87	03	99	05	84	17	86
SMF	24.	50.	132	290	584	106	395	533	116	33.	68.	126	333	641	140	398	803	145
A2	753	885	.19	.76	.13	6.4	1.8	0.9	61.	694	568	.04	.32	.74	8.3	7.9	7.1	78.
	1	95	87	42	34	63	06	21	38	3	63	58	31	27	33	6	66	47
SGM	24.	49.	128	260	525	954	312	436	940	34.	69.	128	316	609	130	307	608	108
FA2	009	387	.12	.10	.85	.56	2.7	1.5	6.5	147	301	.63	.26	.32	9.5	6.0	7.8	75.
	02	24	55	31	63	19	75	87	45	84	51	35	27	37	46	73	65	5
SHM	23.	46.	125	302	603	109	416	553	120	33.	67.	124	347	672	147	424	860	154
FA2	404	816	.71	.79	.04	0.4	7.8	8.3	19.	171	305	.91	.31	.80	1.1	0.9	6.4	07.
	23	96	17	45	51	11	01	83	06	74	38	11	33	67	14	79	15	76
SMIN	15.	29.	72.	179	339	552	224	300	602	22.	43.	77.	216	407	858	269	544	893
FA1	746	807	709	.92	.70	.32	3.7	9.1	4.7	184	053	230	.65	.84	.04	7.0	6.7	9.4
	42	49	03	06	59	75	74	96	08	04	59	27	77	17	31	31	83	88
SMA	12.	21.	47.	124	225	309	139	187	344	15.	28.	44.	140	247	469	178		488
XFA1	010	911	241	.16	.67	.46	3.9	5.1	8.0	237	333	729	.53	.38	.54	7.6	351	5.7
	21	89	18	53	03	1	15	37	91	74	08	84	46	3	75	93	2.9	81
SMID	12.	22.	47.	124	225	309	139	187	344	15.	28.	45.	140	247	469	178	351	488
FA1	090	174	953	.25	.91	.94	4.0	5.4	8.7	340	524	221	.64	.58	.94	7.8	3.0	6.2
	06	48	2	6	39	11	83	74	59	99	45	06	45	63	28	05	92	24
SMF	13.	26.	59.	144	274	438	169	240	496	18.	35.	56.	168	300	617	207	407	629
A1	493	858	041	.93	.97	.66	2.7	9.3	0.5	155	059	316	.82	.93	.47	0.4	4.7	8.9
	96	38	53	46	85	03	34	47	9	87	91	67	23	46	61	72	95	34
SGM	12.	24.	53.	129	237	334	142	193	358	19.	37.	63.	152	272	524	181	356	501
FA1	770	044	167	.26	.35	.92	9.4	5.6	5.0	631	656	798	.77	.24	.23	5.9	9.9	8.7
	39	66	21	53	76	34	07	75	05	9	75	35	32	77	63	45	62	45
SHM	12.	22.	51.	195	369	599	388	498		16.	31.	51.	251	477	103	405	824	146
FA1	447	715	135	.39	.88	.82	7.0	8.4	108	792	881	738	.89	.36	6.1	8.7	7.1	93.
	69	28	75	1	98	4	02	63	67	49	37	6	83	1	91	48	84	58
LTSM	25.	51.	135	301	600	108	410	545	118	34.	70.	130	344	667	145	418	849	152
INFA	410	468	.15	.05	.05	6.2	3.8	7.4	38.	539	113	.61	.73	.91	9.4	4.2	0.2	04.
2	93	62	26	12	7	28	12	82	65	5	97	21	74	33	5	88	37	6
LTSM	19.	40.	167	346	572	208	290	618	24.	48.	90.	191	363	722	221	419	762	
AXFA	163	926	103	.22	.49	.44	8.4	0.8	0.1	385	780	555	.75	.88	.34	9.0	1.5	6.9
2	4	7	.41	65	1	76	2	51	4	91	62	75	92	47	58	44	61	
LTSM	20.	44.	113	174	363	608	210	292	622	27.	54.	100	200	380	753	222	420	765
IDFA	989	490	.52	.49	.48	.10	2.0	5.7	5.9	058	053	.72	.53	.36	.67	8.5	6.9	9.7
2	04	68	91	25	04	94	26	43	34	31	31	95	44	06	73	84	26	11



Global Journal of Engineering Science and Research Management

LTSM	24.	50.	132	291	585	106	396	534	116	33.	68.	126	334	644	141	400	806	146
FA2	813	949	.54	.78	.97	8.4	8.8	4.5	83.	744	722	.49	.37	.43	2.9	4.7	7.7	51.
LTSG	24.	49.	129	265	538	975	331	457	995	34.		128	319	617	132	323	633	118
MFA	154	608	.05	.88	.48	.68	1.5	3.7	7.0	172	69.	.81	.58	.15	7.8	4.4	2.0	16.
2	91	93	5	22	62	7	56	28	45	386	15	98	25	73	17	14	89	
LTSH	23.	47.	127	302	603	109	416	553	120	33.	67.	125	347	672	147	424	860	154
MFA	618	428	.07	.84	.18	0.7	7.8	8.4	19.	261	564	.43	.33	.84	1.1	0.9	6.4	07.
2	77	47	64	76	86	13	07	01	1	37	61	15	42	88	94	81	17	77
LTSM	17.	34.		202	405	695	267	363	774	23.	48.	89.	241	465	974	292	577	104
INFA	422	495	89.	.44	.81	.41	5.2	2.2	4.9	756	534	293	.03	.64	.45	9.2	5.8	44.
1	36	79	591	41	22	68	81	36	09	83	58	3	08	63	65	73	1	43
LTSM	14.	28.	73.	159	328	536	207	287	613	18.	37.	66.	182	347	691	221	417	759
AXFA	410	665	135	.85	.76	.84	5.5	7.4	7.0	105	556	256	.81	.35	.92	0.0	6.8	5.8
1	78	89	61	8	06	63	98	09	13	59	81	26	09	64	15	02	39	95
LTSM	14.	28.	73.	159	328	537	207	287	613	18.	37.	66.	182	347		221	417	759
IDFA	479	869	585	.92	.93	.17	5.7	7.6	7.4	193	702	619	.89	.51	692	0.0	6.9	6.2
1	66	84	59	85	3	45	28	45	48	71	88	11	66	37	.21	96	92	17
LTSM	15.	32.	80.		362	621	228	323	708	20.	42.	74.	204	387	798	243	462	859
FA1	630	343	684	175	.21	.60	8.6	4.1	1.4	475	574	505	.62	.44	.00	4.7	7.1	6.4
7	85	81	.61	94	33	23	14	51	9	67	82	42	03	78	9	05	21	
LTSG	15.	30.	76.	163	336	553	210	291	622	21.	44.	79.	192	366	731	223	422	769
MFA	045	277	907	.75	.85	.94	2.1	9.0	5.0	668	504	775	.30	.13	.19	3.1	2.2	1.9
1	51	57	27	71	53	36	51	49	46	48	02	91	14	99	07	9	3	18
LTSH	14.	29.	75.	214	425	725	391	505	110	19.	40.	71.	266	512	111	406	826	147
MFA	772	275	633	.64	.67	.31	1.7	3.3	17.	418	196	175	.99	.29	0.6	7.6	1.1	39.
1	06	05	55	04	34	81	39	32	16	81	34	75	53	26	44	95	37	78
LMS	25.	51.	135	301	600	108	410	545	118	34.	70.	130	344	667	145	418	848	152
MINF	412	465	.14	.05	.01	6.2	3.8	6.9	38.	538	107	.61	.71	.86	9.5	4.1	9.9	03.
A2	72	7	43	25	94	12	87	04	46	94	32	17	89	24	35	04	45	8
LMS	19.	40.	101	173	336	557	208	282	614	24.	48.	90.	185	353	749	212	413	741
MAX	383	703	.83	.99	.65	.80	1.8	4.9	8.6	186	276	120	.87	.68	.56	2.3	7.0	2.9
FA2	81	96	66	87	28	38	07	56	18	31	22	3	85	61	16	31	64	4
LMS	21.	44.	112	180	354	594	209	285	619	26.	53.	100	194	370	780	213	415	744
MID	127	356	.66	.82	.65	.47	6.0	0.7	5.1	952	668	.45	.89	.54	.86	2.1	2.7	5.8
FA2	93	5	88	83	64	05	25	86	43	99	48	91	59	42	17	5	38	72
LMS	24.	50.	132	291	585	106	396	534	116	33.	68.	126	334	643	141	400	806	146
MFA	822	942	.49	.80	.77	8.4	9.5	2.2	83.	741	691	.48	.23	.97	3.6	2.4	4.2	44.
2	86	24	92	72	18	18	07	11	01	49	21	25	2	39	7	48	19	03
LMS	24.	49.	128	266	537	974	331	455	993	34.	69.	128	319	615	133	320	630	117
GMF	177	584	.93	.32	.13	.40	7.6	0.7	9.5	170	368	.80	.15	.89	1.0	0.3	9.7	08.
A2	11	28	36	12	88	56	44	07	67	8	04	9	9	56	81	73	08	5
LMS	23.	47.	126	302	603	109	416	553	120	33.	67.	125	347	672	147	424	860	154
HMF	643	355	.87	.84	.17	0.7	7.8	8.3	19.	249	525	.39	.33	.84	1.2	0.9	6.4	07.
A2	75	73	73	54	59	09	07	97	1	62	59	81	15	11	03	8	17	77
LMS	17.	34.	86.	206	399	684	268	358	771	23.	48.	88.	237	458	994	287	574	102
MINF	713	107	815	.66	.22	.85	1.6	0.6	6.5	530	024	831	.15	.25	.68	4.6	7.9	73.
A1	7	65	75	77	78	83	46	48	02	53	26	92	66	66	61	23	03	43
LMS	14.	28.	68.	166	318	521	206	280	610	17.	36.	64.	176	336	718	211	412	738
MAX	801	129	401	.97	.04	.18	8.3	0.5	4.5	606	719	999	.75	.72	.68	3.0	2.0	1.5
FA1	71	85	4	84	08	13	58	83	72	35	13	49	89	22	61	19	96	3
LMS	14.	28.	68.	167	318	521	206	280	610	17.	36.	65.	176	336	718	211	412	738
MID	865	336	917	.04	.21	.52	8.4	0.8	5.0	696	869	372	.84	.88	.98	3.1	2.2	1.8
FA1	64	38	92	59	7	31	93	29	17	74	58	1	58	41	3	16	52	57
LMS	15.	31.	76.	181	353	608	228	316	705	20.	41.	73.	199	377	824	234	458	837
MFA	978	897	954	.87	.32	.38	8.7	9.6	3.0	088	902	584	.11	.78	.60	7.5	1.9	9.6
1	43	12	03	21	17	94	13	59	8	15	15	06	92	92	83	01	52	68
LMS	15.	29.	72.	170	326	538	209	284	619	21.	43.	79.	186	355	758	213	416	747
GMF	408	774	703	.70	.46	.81	6.1	3.8	4.2	342	888	055	.43	.99	.43	6.9	8.3	8.1
A1	75	85	23	59	58	94	56	43	43	93	63	07	54	08	71	04	43	33
LMS	15.	28.	71.	217	419	717	391		110	18.	39.	70.	265	508	111	406	826	147
HMF	133	742	173	.33	.82	.16	1.7	504	15.	957	417	061	.19	.28	9.3	6.7	0.1	36.
A1	47	97	3	29	34	38	95	4.1	28	08	8	82	37	36	17	87	88	75



Global Journal of Engineering Science and Research Management

LAD	25.	51.	135	300	599	108	409	545	118	34.	70.	130	344	667	145	418	848	151
MINF	385	420	.03	.75	.44	5.3	9.8	2.3	28.	514	058	.52	.47	.42	8.5	0.7	3.6	93.
A2	85	14	7	65	6	93	35	8	11	34	3	74	86	17	36	16	95	54
LAD	13.	33.	80.	14.	34.	54.	24.	19.	21.	15.	28.	57.	17.	26.	40.	25.	13.	14.
MAX	745	367	261	787	080	544	605	461	998	809	726	409	785	733	875	607	354	103
FA2	11	2	73	62	13	84	56	21	91	8	64	73	79	03	34	84	41	04
LAD	18.	40.	101	32.	79.	136	41.	48.	64.	21.	41.	80.	39.	65.	105	36.	26.	37.
MID	008	820	.74	568	923	.77	479	923	848	933	643	473	841	099	.78	781	023	932
FA2	16	49	82	87	55	1	73	27	84	88	76	25	9	81	24	69	51	57
LAD	24.	50.	132	289	582	106	393	531	116	33.	68.	125	331	638	140	395	795	145
MFA	664	824	.00	.40	.46	5.2	5.9	9.1	50.	574	407	.62	.91	.61	3.8	2.8	2.8	20.
2	4	95	23	68	92	57	84	88	37	84	54	6	86	73	19	93	95	5
LAD	23.	49.	127	248	509	937	283	405	891	34.	69.	128	310	598	128	249	479	948
GMF	758	136	.50	.59	.75	.02	1.3	8.1	3.7	095	219	.48	.65	.62	5.6	5.3	1.8	8.2
A2	53	17	48	81	54	62	97	88	47	26	43	13	93	68	49	71	16	83
LAD	22.	45.	124	302	602	109	416	553	120	32.	66.	124	347	672	147	424	860	154
HMF	880	767	.43	.73	.92	0.2	7.7	8.3	19.	966	953	.37	.29	.76	1.0	0.9	6.4	07.
A2	99	94	9	84	48	45	97	71	05	85	47	16	08	52	57	76	11	75
LAD	9.1	16.	45.	105	200	354	139		375	14.	28.	54.	145	280	610	176	355	638
MINF	108	705	486	.73	.40	.88	6.8	182	9.7	272	090	403	.92	.44	.53	2.6	7.6	1.5
A1	85	67	87	94	88	3	45	2.7	41	6	45	43	58	13	67	45	58	44
LAD	0.6	0.8	1.2	1.7	1.2	0.8	13.	4.1	2.0	0.4	0.3	0.5	1.5	0.7	0.5	18.	6.2	2.7
MAX	853	149	088	138	177	575	944	757	280	539	645	154	388	657	559	343	881	610
FA1	47	45	97	38	59	89	07	23	39	21	57	01	53	57	34	78	82	01
LAD	0.8	1.1	2.0	1.7	1.3	1.1	14.	4.3	2.3	0.5	0.5	0.8	1.6	0.8	0.6		6.3	2.9
MID	133	544	893	711	562	157	045	468	889	606	051	976	000	420	855	18.	497	024
FA1	24	98	08	38	65	12	69	66	56	92	94	93	37	2	91	403	97	36
LAD	3.9	10.	20.	35.	76.	169	439	752	200	5.8	12.	17.	50.	82.	206	501	882	195
MFA	146	423	529	431	380	.97	.50	.60	1.2	513	062	821	606	632	.50	.27	.76	3.4
1	46	87	33	26	79	38	15	26	48	83	97	36	51	11	07	46	42	9
LAD	2.2	4.4	10.	7.3	12.	19.	41.	39.		8.9	17.	31.	19.	31.	58.	43.	42.	70.
GMF	276	820	039	970	221	564	655	941	63.	648	339	013	074	640	116	168	730	506
A1	53	32	27	63	53	51	43	92	844	85	54	67	06	11	27	25	19	44
LAD	1.2	1.5	4.5	138	255	428	386	492	107	2.9	5.2	8.6	211	403	908	404	822	146
HMF	921	926	979	.07	.72	.80	2.4	0.9	70.	590	589	607	.86	.51	.68	3.3	0.0	56.
A1	46	21	15	91	41	95	08	38	45	02	44	46	51	85	56	55	18	94

Table 9: AMSE of the estimators when $n = 100$ and $\sigma_{outlier}^2$ (magnitude of outliers) = 250

ESTI MAT ORS	NUMBER OF EXPLANATORY VARIABLES																	
	3									5								
	DEGREES OF MULTICOLLINEARITY									DEGREES OF MULTICOLLINEARITY								
	0.900			0.990			0.999			0.900			0.990			0.999		
	% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS			% OF OUTLIERS		
	10	20		10	20		10	20		10	20		10	20		10	20	
	5%	%	%	5%	%	%	5%	%	%	5%	%	%	5%	%	%	5%	%	%
OLS	150	342	805	174	366	650	214	340	840	208	436	782	223	480	786	214	512	117
	.91	.57	.52	7.4	1.6	7.2	75.	70.	14.	211	.10	.30	6.3	2.6	7.7	217	11.	027
	55	64	94	55	8	55	5	05	76	.75	87	67	31	86	16	18	32	.6
MMI NFA2	148	336	792	171	360	640	211	335	826	208	436	782	223	480	786	214	512	117
	.43	.32	.31	9.2	0.9	0.7	13.	07.	11.	.84	.03	.30	4.5	3.6	8.3	15.	504	290
	4	98	68	32	71	34	36	06	43	49	62	6	72	83	49	25	60	.3
MMA XFA2	103	239	538	619	127	274	486	105	290	114	256	498	639	157	330	533	140	421
	.78	.25	.58	.71	7.5	1.2	6.4	79.	01.	.25	.23	.95	.16	5.2	5.4	6.4	99.	73.
	6	12	01	78	38	51	44	11	89	52	02	44	98	81	45	08	93	47
MMI DFA2	119	273	619	750	151	307	497	107	293	137	303	577	709	175	358	540	142	424
	.27	.87	.19	.06	5.7	2.0	8.0	75.	55.	.14	.58	.95	.43	8.3	9.2	8.0	64.	07.
	66	53	46	59	59	99	69	94	61	15	12	37	89	37	39	31	8	22
MMF A2	145	335	777	168	350	626	205	325	802	201	422	760	215	457	758	205	468	106
	.76	.21	.79	1.1	8.1	0.5	71.	25.	30.	.35	.97	.38	0.8	1.3	1.3	08.	92.	638
	52	43	09	71	62	45	5	23	37	12	19	47	6	6	42	36	58	.2
MGM FA2	141	323	750	153	317	568	158	258	634	205	430	771	199	428	720	149	330	762
	.18	.28	.67	3.6	6.2	8.0	63.	84.	48.	.11	.02	.51	9.6	7.6	5.4	79.	42.	20.
	75	46	91	85	02	37	24	92	54	42	47	87	6	33	4	85	73	24



Global Journal of Engineering Science and Research Management

MHM	135	309	738	172	362	642	214	340	839	200	417	747	225	484	792	217	511	116
FA2	.20	.18	.16	6.8	0.9	4.3	5.4	27.	27.	.20	.23	.53	3.3	6.3	6.7	05.	86.	973
MMI	81.	177	453	875	184	363	100	178	453	121	257	477	124	274		118	286	704
NFAI	245	.94	.07	.51	0.8	1.3	32.	21.	72.	.51	.73	.98	7.7	0.0	489	66.	22.	46.
MMA	55	95	46	21	45	16	55	52	52	01	07	88	75	29	5.6	55	21	53
XFAI	56.	123	319	475	101	239	476	103	286	66.	147	295	573	139	301	526	139	419
MMI	197	.29	.64	.30	8.2	5.3	2.9	94.	68.	413	.61	.35	.47	2.8	1.5	9.4	45.	49.
DFAI	79	35	75	28	18	84	21	6	18	42	7	56	08	03	78	21	54	89
MMI	56.	125	322	476	102	239	476	103	286	67.		298	574	139	301	527	139	419
DFAI	856	.00	.70	.55	0.5	8.4	3.9	96.	71.	015	149	.51	.07	4.4	4.4	0.1	47.	52.
MMF	78	39	3	49	87	74	56	45	55	11	.07	73	25	82	35	1	13	22
A1	68.	170	386	664	138	298	711	134	355	85.	190	370	820	180	368	751	176	488
FAI	526	.40	.71	.16	1.7	1.9	9.8	74.	87.	915	.75	.89	.74	1.7	5.8	7.3	52.	49.
MGM	17	76	83	67	39	96	81	36	08	67	17	8	16	55	61	74	61	61
FAI	61.	139	349	522	111	253	499	107	294	96.	213	405	668	157	332	548	143	426
FAI	929	.60	.82	.79	1.8	2.2	6.6	57.	19.	310	.88	.84	.35	9.8	5.9	3.5	60.	91.
MHM	87	4	64	84	92	85	26	66	82	11	47	04	26	84	63	29	7	75
FAI	58.	130	340	951	204	378	196	306	768	78.	171	332	154	341	558	205	489	112
FAI	981	.89	.89	.26	8.6	9.0	46.	39.	44.	744	.63	.87	7.5	9.1	9.4	97.	71.	291
MM	99	42	6	24	52	67	74	62	52	99	31	84	4	97	93	48	07	.7
MINF	148		792	171	360	639	211	335	825	208	435	782	223	480	786		504	115
A2	.42	336	.13	9.1	0.5	8.8	12.	02.	92.	.83	.97	.12	4.4	3.1	6.2	214	54.	258
MM	33	.29	41	28	7	11	73	13	52	3	67	85	41	15	51	14	25	.9
MAX	101	232	489	541	100	149	430	657	139	108	227		529	103	165	408	848	171
FA2	.65	.84	.10	.02	0.3	8.0	6.9	0.9	06.	.45	.66	430	.77	4.7	0.8	9.2	1.5	76.
MM	07	74	5	22	22	49	28	45	88	01	27	.94	51	29	18	96	47	46
MID	118	270	592	684	127	197	442	679	143	133	285	536	606	125	207	417	866	174
FA2	.12	.57	.25	.37	4.8	5.0	5.2	8.8	75.	.13	.08	.15	.89	4.3	8.6	1.0	7.4	79.
MM	6	82	22	03	63	77	59	25	1	4	16	27	84	33	5	92	21	91
MFA	145	335	777	168	350		205	324	800	201	422	758	214	456	755	204	467	
2	.72	.15	.01	0.6	5.7	625	67.	90.	99.	.21	.41	.90	9.3	1.4	6.7	91.	26.	105
MMG	12	96	17	21	41	0.6	81	11	14	17	81	24	62	54	35	09	67	673
MFA	141	322	747	152	315	559	157	251	604	205	429	770	199	425	712	146	309	659
2	.04	.94	.79	8.7	5.5	1.4	61.	38.	38.	.05	.79	.84	3.1	3.6	2.0	67.	86.	71.
MMH	2	2	11	56	09	65	15	49	57	27	49	63	65	26	19	44	81	95
MFA	134	308	734	172	362	642	214	340	839	200	416	745	225	484	792	217	511	116
2	.87	.28	.04	6.7	0.7	3.3	5.4	27.	27.	.07	.53	.30	3.3	6.2	6.4	05.	511	973
MM	77.	165	376	821	165	278	971	155	366	116	229	402	119	244	402	113	257	578
MINF	623	.09	.52	.86	0.9	8.9	0.1	00.	45.	.27	.48	.59	4.1	1.1	1.7	15.	40.	89.
A1	2	86	07	58	56	14	17	76	67	98	78	38	61	05	43	15	64	52
MM	51.	104	205	379	709	102	419	636	134	56.	96.	154	458	821	123	401	831	168
MAX	039	.88	.20	.46	.00	0.6	6.6	4.6	76.	890	516	.63	.03	.41	5.5	2.5	0.5	96.
FA1	43	43	67	09	89	81	02	61	06	88	08	74	86	1	91	32	31	52
MM	51.	106	208	380	711	102	419	636	134	57.	98.	158	458	823	123	401	831	168
MID	763	.73	.86	.93	.53	4.6	7.7	6.6	80.	543	221	.64	.69	.28	9.1	3.3	2.2	99.
FA1	98	37	88	61	38	4	08	82	35	06	71	59	19	44	27	23	68	38
MM	64.	156	289	589	112	184	666	101	230	77.	148	256	729	130	222	654	126	268
MFA	149	.73	.34	.96	0.1	4.4	9.2	18.	62.	885	.18	.42	.16	6.6	5.0	1.0	57.	35.
1	94	68	2	93	28	02	69	41	82	03	14	56	28	54	36	9	29	6
MMG	57.	122	242	433	812	120	444	677	144	89.	176	304	561	104	168	425	877	178
MFA	185	.68	.21	.62	.03	4.1	4.8	7.4	61.	086	.18	.26	.78	0.2	1.4	7.0	6.6	60.
1	96	95	1	04	91	62	85	15	03	33	99	81	01	2	47	8	31	25
MMH	54.	113	231	904	189	304	196	304	764	70.	125	205	151	327	504	205	489	112
MFA	149	.18	.67	.31	8.4	9.0	30.	92.	16.	366	.97	.31	5.8	7.2	2.1	84.	30.	113
1	79	78	53	54	35	91	33	09	95	36	2	63	21	21	89	2	38	.3
SMA	148	336	792	171	360	639	211	335	826	208	436	782	223	480	786	214	504	115
FA2	.46	.37	.24	9.7	1.5	9.8	19.	09.	06.	.90	.07	.27	5.2	4.5	7.8	21.	71.	284
SMIN	88	81	76	25	28	14	27	35	03	84	11	29	16	18	4	04	.4	
FA2	109	246	517	818	151	225	830	112	243	131	268	486	101	204	292	870	194	382
XFA2	.47	.01	.31	.56	4.6	5.5	8.8	89.	29.	.35	.05	.20	1.8	5.3	6.1	2.7	12.	53.
FA2	24	63	91	01	52	38	4	85	04	57	41	35	89	71	71	47	75	77



Global Journal of Engineering Science and Research Management

SMID	122	277	607	922	172	263	839	114	247	149	311	570	106	219	324	876	195	384
FA2	.41	.40	.88	.60	3.1	8.8	5.2	70.	12.	.17	.13	.03	2.7	6.1	3.9	0.3	54.	96.
SMF	145	335	777	168	351	625	206	325	801	201	423	760	215	458	757	205	471	106
A2	.90	.28	.48	3.5	1.2	5.9	04.	38.	95.	.91	.30	.09	7.7	3.7	5.4	83.	44.	459
SGM	141	323	749	155	319	564	165	260	626	205	430	771	202	432	718	160	352	744
FA2	.62	.67	.53	2.0	8.5	4.9	96.	34.	18.	.36	.17	.38	7.3	5.0	6.0	47.	12.	96.
SHM	136	310	736	172	362	642	214	340	839	200	417	747	225	484	792	217	511	116
FA2	.00	.17	.36	7.0	1.1	3.8	54.	27.	27.	.76	.80	.10	3.4	6.4	6.7	05.	86.	973
SMIN	90.	191	419	102	200	329	121	181	427	136	269	463	145	300	469	136	315	683
FA1	881	.58	.42	1.7	6.8	1.4	23.	48.	96.	.99	.40	.89	0.6	1.3	7.7	50.	08.	56.
SMA	69.	143	268	701	128	185	822	111	239	93.	172	270	962	189	260	864	192	380
XFA1	274	.26	.11	.36	4.6	8.5	6.9	19.	74.	894	.09	.74	.86	0.9	6.9	7.9	78.	23.
SMID	69.	144	271	702	128	186	822	111	239	94.	173	273	963	189	260	864	192	380
FA1	889	.80	.39	.38	6.7	2.0	7.8	21.	77.	374	.36	.96	.32	2.4	9.8	8.5	79.	25.
SMF	80.	184	343	854	160	253	997	139	317	109		350	114	223	335	103	223	453
A1	207	.93	.18	.19	5.9	4.1	5.8	79.	47.	.26	209	.04	2.5	1.7	2.3	64.	74.	36.
SGM	74.	.80	.34	.13	8.4	5.3	9.4	53.	82.	.38	.21	.13	3.0	9.1	9.0	0.2	36.	93.
FA1	481	55	47	81	56	38	53	97	53	71	97	29	88	9	53	2	15	59
SHM	71.	150	291	107	218	349	197	306	767	103	193	309	166	356	546	206	490	112
FA1	646	.03	.37	2.1	4.4	4.1	57.	95.	05.	.37	.52	.86	5.0	7.6	6.6	52.	33.	260
LTSM	148	336	792	172	360	640	211	335	826	208	436	782	223	480	787	214	504	115
INFA	2	.54	.09	.76	59	77	05	65	43	54	56	57	13	11	7	64	42	72
AXFA	115	263	581	101	203	344	114	168	420	145	306	554	122	253	407	115	259	549
2	.50	.97	.16	6.3	6.0	0.0	05.	69.	32.	.92	.45	.32	2.9	3.5	9.8	77.	86.	70.
LTSM	126	287	645	109	218	368	114	170	423	159	337	614	126	265	430	116	260	551
IDFA	2	.13	.66	.35	1.3	1.8	7.6	68.	03.	.64	.69	.31	2.4	4.1	5.7	19.	95.	48.
FA2	14	92	35	59	63	92	41	57	14	14	39	51	92	22	42	14	93	5
LTSM	146	335	779	168	352	627	206	326	804	202	424	762	216	460	760	206	475	107
FA2	.15	.55	.03	6.8	1.2	0.9	52.	42.	81.	.51	.67	.30	5.2	6.5	4.2	59.	03.	485
LTSG	142	325	754	157	326	576	173	274	671	205	430	772	205	438	727	170	379	820
MFA	2	.34	.14	.70	2.7	0.3	4.2	96.	39.	72.	.65	.79	.44	0.8	4.8	1.2	10.	50.
2	24	1	04	26	02	83	58	79	46	06	06	74	99	22	65	66	02	99
LTSH	137	313	743	172	362	642	214	340	839	201	419	750	225	484	792	217	511	116
MFA	2	.44	.65	.73	7.4	1.9	5.7	54.	27.	.44	.51	.45	3.5	6.6	7.2	05.	86.	973
2	54	96	67	16	86	17	31	01	8	05	58	74	63	67	41	29	03	.4
LTSM	100	224	514	116	238	411	141	217	540	150	307	538	157	330	535	152	351	773
INFA	1	.29	.34	.06	3.4	1.2	2.0	25.	56.	10.	.25	.42	.52	0.4	4.0	2.1	01.	74.
1	11	55	67	34	72	87	99	42	1	57	86	61	55	41	99	15	78	43
LTSM	82.	189	412	930	187	318	113	167	417	116	236	400	118	241	384	115	258	548
AXFA	1	514	.60	.19	.63	4.3	1.3	45.	42.	76.	.87	.37	.46	4.9	0.7	7.1	37.	82.
1	28	15	02	87	42	16	75	15	28	26	11	96	78	42	13	04	38	66
LTSM	83.	190	414	931	187	318	113	167	417	117	237	402	118	241	384	115	258	548
IDFA	1	017	.72	.44	.43	5.8	3.6	46.	43.	78.	.25	.32	.88	5.3	1.9	9.3	37.	83.
1	17	95	85	36	73	62	35	44	88	85	85	4	43	21	5	46	47	42
LTSM	91.	219	462	104	209	362	125	188	469	128	264	457	132	268	438	127	282	601
FA1	521	.57	.74	2.0	9.8	0.0	99.	16.	18.	.92	.21	.87	4.9	2.6	2.6	96.	10.	71.
1	47	9	55	31	95	38	68	7	02	27	32	66	01	85	87	55	99	58
LTSG	86.	200	434	959	193	328	114	169	423	135	279	484	123	253	409	116	261	553
MFA	1	797	.12	.70	.66	3.6	4.1	78.	91.	50.	.19	.06	.23	9.4	6.5	6.2	62.	66.
1	97	44	12	09	29	84	74	13	86	31	54	2	46	56	16	9	53	59



Global Journal of Engineering Science and Research Management

LTSH	84.	194	427	120	250	424	199	310	775	124	251	428	174	374	591	207	491	112
MFA	411	.48	.93	1.0	3.4	4.2	06.	50.	11.	.22	.75	.30	9.7	7.8	5.1	13.	38.	498
1	26	06	27	84	75	84	7	35	31	48	06	72	93	74	01	36	69	.8
LMS	148	336	792	172	360	640	211	335	826	208	436	782	223	480	787	214	504	115
MINF	.53	.56	.64	0.4	3.2	2.5	27.	26.	54.	.96	.24	.57	6.0	5.9	0.4	26.	87.	325
A2	3	78	67	75	2	63	72	78	07	25	71	86	35	5	07	99	42	.8
LMS	115	261	582	100	196	334	105	173	408	142	302	550	122	252	396	108	252	539
MAX	.88	.88	.19	9.7	6.8	3.9	48.	12.	53.	.19	.05	.84	2.1	3.8	2.8	81.	96.	84.
FA2	05	23	56	97	41	39	45	62	67	11	48	32	03	43	25	83	84	4
LMS	126	286	645	108	211	360	106	174	411	156	334	611	126	264	419	109	254	541
MID	.18	.58	.74	4.9	7.5	3.6	13.	42.	29.	.92	.55	.85	2.5	2.7	6.7	26.	08.	67.
FA2	35	32	91	6	28	54	45	84	24	65	6	96	21	07	04	89	32	94
LMS	146	335	779	168	206	326	804	202	424	762	216	460	760	206	474	107	373	107
MFA	.13	.53	.05	6.9	351	8.9	46.	45.	81.	.43	.55	.28	4.6	1.6	0.4	41.	60.	373
2	78	59	97	2	9.9	81	12	59	89	08	91	71	43	88	88	34	17	.3
LMS	142	325	754	157	325	575	171	275	668	205	430	772	205	437	726	167	376	814
GMF	.29	.02	.74	2.5	1.6	0.8	98.	52.	80.	.62	.74	.45	0.7	4.6	0.0	28.	47.	61.
A2	57	73	76	62	74	56	51	16	03	26	92	3	57	66	93	77	33	66
LMS	137	313	743	172	362	642	214	340	839	201	419	750	225	484	792	217	511	116
HMF	.45	.32	.81	7.4	1.8	5.5	54.	28.	27.	.36	.36	.52	3.5	6.6	7.2	05.	86.	973
A2	04	22	57	16	98	06	3	01	8	82	8	47	27	34	11	29	03	.4
LMS	101	220	516	115	232	404	135	220	531	146	303	534	157	328	528	147	347	767
MINF	.50	.12	.02	7.6	6.4	4.9	44.	66.	84.	.83	.06	.86	3.9	6.1	0.0	68.	35.	08.
A1	82	68	18	37	49	44	1	8	34	08	97	57	28	79	23	19	78	63
LMS	84.	183	414	923	180	306	104	171	111	230	398	118	240	372	108	251	538	538
MAX	990	.36	.66	.35	2.6	5.0	87.	90.	405	.67	.05	.00	3.0	3.4	4.7	38.	90.	09.
FA1	18	42	75	6	91	94	21	21	91	91	15	24	04	39	58	73	84	3
LMS	85.	184	416	924	180	306	104	171	405	112	231	400	118	240	372	108	251	538
MID	473	.55	.96	.18	4.2	7.7	87.	91.	93.	.07	.03	.35	3.3	4.5	6.9	39.	91.	11.
FA1	1	77	87	67	33	51	83	45	67	37	67	85	8	84	94	18	94	12
LMS	93.	215	465	103	203	353	118	192	458	124	258	454	132	267	427	121	276	592
MFA	380	.08	.31	5.4	2.5	2.9	34.	13.	51.	.18	.48	.26	6.1	0.8	6.4	66.	12.	72.
1	6	36	56	59	57	58	76	69	14	07	82	13	02	8	85	76	23	01
LMS	89.	194	437	952	186	317	106	174	411	130	273	480	123	252	397	109	254	543
GMF	015	.49	.38	.97	2.5	8.0	24.	30.	79.	.77	.73	.40	8.9	6.8	9.6	73.	72.	91.
A1	8	42	75	87	23	83	18	76	03	97	8	49	58	39	9	58	59	81
LMS	86.	188	430	119	246	417	198	310	774	119	245	426	174	373	587	207	491	112
HMF	852	.51	.43	7.9	5.7	6.6	83.	67.	90.	.57	.96	.17	5.6	7.6	0.8	00.	29.	477
A1	18	19	.57	63	78	54	29	03	67	64	61	75	69	04	98	89	33	.2
LAD	148	336	792	171	360	639	211	334	825	208	435	782	223	480	786	214	504	115
MINF	.39	.01	8.8	0.0	8.0	09.	97.	81.	.79	.92	.04	4.1	2.6	5.4	11.	48.	246	246
A2	02	.19	79	45	45	81	07	79	93	52	8	13	2	45	35	25	.4	.4
LAD	89.	205	427	180	300	445	34.	58.	90.	77.	178	362	55.	179	341	23.	38.	45.
MAX	265	.33	.23	.56	.38	.53	179	193	249	407	.79	.44	029	.41	.85	149	632	724
FA2	26	36	57	63	83	82	85	81	72	6	71	34	31	75	42	91	11	45
LAD	112	258	564	386	674	104	92.	183	294	113	257	499	145	445	844	58.	124	154
MID	.63	.43	.00	.88	.15	8.9	695	.46	.70	.97	.29	.41	.22	.52	.88	708	.37	.46
FA2	99	11	47	54	39	24	45	19	7	57	78	53	65	47	88	7	36	13
LAD	145	335	776	167	350	624	205	324	800	200	421	758	214	455	754	204	465	105
MFA	.57	.02	.48	9.0	2.3	6.5	47.	51.	18.	.78	.90	.15	5.1	1.9	5.5	49.	30.	105
2	86	07	81	75	79	75	52	58	89	75	09	28	08	24	96	63	186	186
LAD	140	321	745	151	312	554	150	240	577	204	429	770	197	421	707	135	278	579
GMF	.53	.98	.66	3.0	1.8	2.9	24.	15.	84.	.88	.59	.52	1.3	7.5	7.9	52.	31.	45.
A2	23	71	97	34	69	72	64	24	24	07	13	44	04	66	11	31	19	83
LAD	132	304	728	172	362	642	214	340	839	199	415	743	225	484	792	217	511	116
HMF	.56	.59	.70	6.5	0.4	2.8	54.	27.	27.	.51	.57	.62	3.2	6.1	6.2	05.	85.	973
A2	99	31	69	75	82	34	24	85	54	27	39	69	58	88	91	26	99	.3
LAD	49.	96.	262	587	119	211	692	112	272	89.	181	324	941	199	331	915	211	477
MINF	776	497	.80	.03	9.9	9.4	8.5	57.	39.	231	.35	.39	.53	9.4	8.3	2.2	37.	13.
A1	33	29	81	39	87	61	83	29	54	85	97	93	11	2	78	64	36	43
LAD	1.8	2.5	4.3	2.3	2.8	3.3	5.6	2.8	3.4	0.9	1.2	2.3	1.2	1.2	1.6	5.8	2.1	1.5
MAX	099	285	418	932	325	505	653	630	956	128	026	876	864	366	368	588	311	889
FA1	21	8	07	28	94	47	92	01	99	54	11	19	19	13	82	72	91	29



Global Journal of Engineering Science and Research Management

LAD	2.7	4.4	8.5	3.1	4.4	5.7	6.1	3.9	5.6	1.3	2.2	5.2	1.4	1.8	2.7	6.0	2.5	2.3
MID	241	724	184	960	429	360	748	532	168	416	307	955	397	309	976	216	849	040
FAI	84	44	76	4	63	39	99	48	99	18	48	97	88	99	81	85	06	91
LAD	24.	82.	125	249	460	879	268	392	946	29.	64.	124	304	512	102	276	446	960
MFA	779	220	.83	.88	.50	.46	0.9	0.8	1.7	695	651	.42	.63	.11	5.7	0.8	1.5	1.2
1	6	32	94	82	61	74	45	98	57	46	79	4	69	19	37	12	81	83
LAD	11.		52.	43.	76.	124	104	169	341	47.	105	190	90.	185	375	110	190	353
GMF	611	25.	269	753	756	.45	.62	.55	.88	388	.17	.06	635	.62	.71	.04	.65	.58
AI	15	547	44	01	48	67	92	38	03	1	21	82	56	33	09	21	46	44
LAD	4.0	8.2	23.	698	152	243	195	303	761	15.	28.	47.	139	307	466	205	488	112
HMF	644	258	106	.64	5.4	4.7	51.	15.	47.	235	627	211	5.2	3.2	6.1	56.	87.	038
AI	05	37	28	53	96	07	95	4	11	06	87	61	91	3	17	34	27	.7